

Driving Japan's Green Transition: An Advanced Modeling Framework for Grid Stability and Renewable Integration

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Abstract

The increasing integration of photovoltaic (PV) systems into Japan's power grid presents significant challenges for grid stability and energy forecasting, primarily due to the intermittent nature of solar power. A key impediment to accurate power output prediction is the difficulty in precisely estimating PV cell parameters from the limited information available on manufacturer datasheets. This study proposes and validates a robust methodology to extract comprehensive PV parameters using advanced metaheuristic optimization for both single-diode and double-diode models. We apply and compare several algorithms, including Best–Worst–Random (BWR), Best-Mean-Random (BMR), and JAYA, utilizing data from three distinct module types: polycrystalline, monocrystalline, and thin-film. The optimization process minimizes the error between the model's calculated I-V characteristics and the empirical data at the open-circuit, short-circuit, and maximum power points. The results demonstrate that the proposed metaheuristic approach successfully identifies optimal parameter sets, achieving a precise match with experimental I-V and P-V curves. This enhanced modeling accuracy provides a reliable foundation for predicting energy production, facilitating more effective grid management and operational planning for Japanese power utilities and supporting the nation's transition to a renewable-centric power system.

Keywords: Best–Worst–Random (BWR) algorithm, Jaya algorithm, Best-Mean-Random (BMR), Parameter estimation, Single-diode model, Double-diode model, Metaheuristic optimization, Energy forecasting, Photovoltaic modeling

1. Introduction

Power generation business are shifting toward renewable energy sources, and substantial research is dedicated to improving their continuous performance Rashid (2024). Japan's power utilities, like those globally, face challenges in maintaining the reliability and maximizing the return on investment of solar photovoltaic installations Hopwood and Gunda (2022). One critical aspect involves accurately modeling PV systems to predict energy production and optimize operational parameters Gayibov and Abdullaev (2021). The intermittent nature of solar energy and the complexities of real-world operating conditions make precise modeling essential for grid stability and economic viability Salazar-Peña et al. (2024). An accurate model is also required to predict the energy available from the array King et al. (2003). The fact that manufacturer datasheets usually only include open-circuit voltage, short-circuit current, and maximum power point characteristics is a major barrier. Ulapane et al. (2012). This necessitates robust parameter estimation techniques that can derive comprehensive PV characteristics from sparse data, enhancing power output prediction and facilitating optimal inverter design Muhsen et al. (2016) Mhanni and Lagmich (2024). To address these issues, enhanced methodologies are needed that improve traditional technologies in terms

of accuracy and prediction precision for PV cell generation Kumar et al. (2024). The automated design of forecasting models is challenged by missing information regarding PV mounting configurations and the limited amount of historical data available for training, especially for new PV plants Meisenbacher et al. (2022). These models are crucial for optimizing the integration of solar energy into the grid and for predicting its performance under varying meteorological conditions Jiang et al. (2023). Accurate forecasting of PV power is crucial for the efficient integration of solar energy into power systems, enabling better planning, scheduling, and operation of the grid Leo et al. (2025). This is particularly important for grid-connected PV systems, those with integrated storage, and systems operating under dynamic demand-response schemes Leo et al. (2025).

Japan market faces unique challenges due to its high solar penetration and complex grid infrastructure, making accurate PV power forecasting and system modeling paramount for ensuring grid stability and optimizing energy resource use Kim et al. (2021) Lari et al. (2025). Accurate forecasting also helps reduce reserve capacity and prevent electrical energy system disruptions Assaf et al. (2023). Given the increasing integration of PV systems into power grids, precise PV output forecasts have become an efficient solution to manage variability and reduce operational costs Nguyen and Müsgens (2021). Therefore, the development of accurate and reliable PV power forecasting techniques is of great importance for maintaining grid stability and optimizing energy resource utilization Leo et al. (2025) Li

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et al. (2021). As solar energy becomes a more significant part of the electricity generation mix, the ability to accurately forecast the energy produced by PV systems becomes increasingly important Konstantinou et al. (2021). As demand for energy increases, integrating alternative energy sources like PV cell into the power grid becomes crucial for ensuring a reliable power supply Kumar et al. (2020) .

2. Background and Motivation

Achieving these objectives requires advanced machine learning algorithms and optimization techniques to manage the inherent unpredictability of PV generation (Soleymani and Mammadzadeh, 2023). Significant work is now being done to develop real-time performance models that use a deployment's location and weather conditions to estimate solar output Chen and Irwin (2017). Japan's focus on strengthening the competitiveness and economic efficiency of thermal power generation, along with its initiatives to secure fuel and necessary installed capacity, highlights the need for accurate PV models to effectively integrate solar energy into the grid Yamazaki and Ikki (2022). Given that PV power generation is highly dependent on weather conditions, precise forecasting is difficult but necessary for stability, dependability, and scheduling of power system operations Iheanetu (2022). Accurate PV power forecasting necessitates identifying and predicting weather conditions impacting PV systems, often employing diverse data preprocessing techniques to enhance prediction capabilities Kohút and Kvasnica (2023) Carrera et al. (2020). To ensure long-term operation and maintenance of existing PV systems, predictive models play a crucial role in achieving the goal of introducing 120 GW of PV power generation by 2030 in Japan Yamazaki and Ikki (2022).

3. Literature Review

With the increasing adoption of renewable energy sources such as PV and wind power, the need for accurate power forecasting methods has become more critical for ensuring the safe and economic operation of power systems Liao et al. (2022). The need for precise PV power calculation for particular geographic areas is further highlighted by the erratic nature of solar energy and its reliance on meteorological factors like solar radiation and ambient temperature Chakraborty et al. (2023). By using statistical and machine learning techniques to anticipate PV production, these predictions can manage variability and lower operating costs related to solar power integration Kohút and Kvasnica (2023) Zhang et al. (2020). Integration of PV in power producing companies requires the use of forecasting models to address reliability issues Riggs et al. (2023). Municipalities are progressively enhancing the deployment of renewable energy by establishing capacity goals, allocating specific promotion zones, installing photovoltaic systems in municipal buildings, and offering financial incentives, signaling a comprehensive move towards embracing solar energy. Yamazaki and Ikki (2022). These efforts are complemented by national

projects aimed at decarbonization and accelerating the adoption of renewable energy sources, which include managing feed-in tariff schemes and promoting new development while reducing costs Yamazaki and Ikki (2022) . Business market of Japan are also developing their solar sectors, especially in manufacturing photovoltaic cells and modules Yamazaki and Ikki (2022).

The goal is to create a stable supply-and-demand power grid systems by modeling solar photovoltaic generation prediction Kim et al. (2021).

Parameter estimation of solar cells using datasheet information with the application of an adaptive differential evolution algorithm" Biswas et al. (2018), details mathematical models for solar cells, specifically focusing on single-diode and double-diode models. The objective of the optimization in this study is to accurately estimate PV cell parameters to satisfy the current-voltage relationships at three major points: open circuit, short circuit, and maximum power points Biswas et al. (2018). Such an estimation is critical because experimental data or detailed characteristic data of a PV module may not always be readily available, making parameter estimation from datasheet values a practical necessity Biswas et al. (2018). For example, models could integrate machine learning techniques and data science tools to predict the power output of building-integrated photovoltaic systems across various building orientations, thereby enhancing the precision of PV power generation forecasts (Kabilan et al., 2021) (Maitanova et al., 2020) and ensemble techniques, like random forest and extreme gradient boosting, are well-suited for solar radiation prediction because they improve stability, reduce variation and bias, and combine several machine learning models (Mishra et al., 2023). Furthermore, improving the accuracy of hourly solar power forecasts can be achieved by including a PV-performance model as part of the data-mining stage (Pombo et al., 2022). This strategy makes it possible to integrate solar energy into current power systems in a more dependable and economical manner (Momenitabar et al., 2020). These evaluations can be further improved by utilizing computer vision and deep learning techniques, particularly in urban settings where comprehensive street-level data may be scarce (Wang, 2024). These methods overcome temporal lags and increase prediction accuracy by extracting pertinent information from sky photos to forecast future PV output (Nie et al., 2023; Misra Palanisamy, 2019). The combination of machine learning and deep learning models can improve short-term solar irradiance forecasts, given the volatility of energy generation due to weather dependence (Carrera et al., 2020) (El-Shahat et al., 2024). A sizable collection of data is frequently used to perform accurate parameter estimation Biswas et al. (2018). This is especially crucial when utilizing evolutionary algorithms to reduce errors and identify the best cell parameters, which may be improved by applying techniques like flower pollination algorithms or particle swarm optimization Biswas et al. (2018).

4. Methodology

Numerical data and mathematical models

The method minimizes inaccuracies in current-voltage relationships at critical points by optimizing all relevant PV cell

characteristics without making any assumptions. Biswas et al. (2018).

Mathematical Model

The single-diode and double-diode models are well-established mathematical models that we used in our study to accurately estimate solar cell properties. Our main goal was to make sure that the current-voltage relationships that were obtained from these models accurately reflected the performance at the open circuit, short circuit, and maximum power points Biswas et al. (2018).

For each model, we distinguished between parameters that were optimized by our chosen algorithm and those that were calculated based on fundamental electrical relationships. The specific parameters involved in our modeling approach include the diode ideality factor (a , a_1 , a_2), series resistance (R_S), parallel resistance (R_{sh}), photo current (I_L), and diode reverse saturation current (I_0 , I_{01} , I_{02}).

The optimized and calculated parameters for each model utilized in our work are summarized in Table 1, drawing inspiration from the parameterization strategies discussed by Biswas et al. (2018):

Table 1: Optimized and Calculated Parameters for PV Models

| Model | Optimized Parameters | Calculated Parameters |
|--------------------|-------------------------------------|-----------------------------|
| Single-diode model | $\{a, R_S, R_{sh}\}$ | I_L [Eq.], I_0 [Eq.] |
| Double-diode model | $\{a_1, a_2, R_S, R_{sh}, I_{01}\}$ | I_{02} [Eq.], I_L [Eq.] |

The formulation of our objective function was critical, and its successful minimization ensured that the derived PV module performance aligned precisely with the empirical I-V characteristics at the three aforementioned major operating points Biswas et al. (2018).

This study's mathematical modeling builds upon foundational research utilizing single-diode and double-diode models. Their work provides an in-depth analysis of comparable circuits for ideal photovoltaic cells and PV modules. Our framework is largely based on their formulations, particularly those explaining the current-voltage behavior. Biswas et al. (2018)

In particular, we build our models using a number of important equations from Biswas et al. (Biswas et al., 2018). These formulas describe how PV cells and modules behave in a variety of scenarios, such as maximum power points, open circuits, and short circuits. As stated in their study, the following formulas are essential to our analysis:

- **The ideal current for PV cells**

$$I = I_{PV,cell} - I_D \text{ (Biswas et al., 2018)}$$

- **I-V characteristic of ideal PV cell**

$$I = I_{PV,cell} - I_{O,cell} \left[\exp \left(\frac{qV}{akT} \right) - 1 \right] \text{ (Biswas et al., 2018)}$$

- **I-V characteristic of single-diode model for PV module**

$$I = I_{PV} - I_O \left[\exp \left(\frac{q(V+R_S I)}{akN_C T} \right) - 1 \right] - \frac{V+R_S I}{R_P} \text{ (Biswas et al., 2018)}$$

- **Open-circuit condition from single-diode model**

$$0 = I_{PV} - I_O \left[\exp \left(\frac{qV_{OC}}{akN_C T} \right) - 1 \right] - \frac{V_{OC}}{R_P} \text{ (Biswas et al., 2018)}$$

- **Photocurrent (I_{PV}) at open-circuit**

$$I_{PV} = I_O \left[\exp \left(\frac{qV_{OC}}{akN_C T} \right) - 1 \right] + \frac{V_{OC}}{R_P} \text{ (Biswas et al., 2018)}$$

- **Short-circuit condition from single-diode model**

$$I_{SC} = I_{PV} - I_O \left[\exp \left(\frac{qR_S I_{SC}}{akN_C T} \right) - 1 \right] - \frac{R_S I_{SC}}{R_P} \text{ (Biswas et al., 2018)}$$

- **Photocurrent (I_{PV}) at short-circuit**

$$I_{PV} = I_{SC} + I_O \left[\exp \left(\frac{qR_S I_{SC}}{akN_C T} \right) - 1 \right] + \frac{R_S I_{SC}}{R_P} \text{ (Biswas et al., 2018)}$$

- **Reverse saturation current (I_O)**

$$I_O = \frac{I_{SC} + \frac{R_S I_{SC}}{R_P} - \frac{V_{OC}}{R_P}}{\exp \left(\frac{qV_{OC}}{akN_C T} \right) - \exp \left(\frac{qR_S I_{SC}}{akN_C T} \right)} \text{ (Biswas et al., 2018)}$$

- **Photocurrent (I_{PV}) derived from open and short-circuit conditions**

$$I_{PV} = \left(I_{SC} + \frac{R_S I_{SC}}{R_P} - \frac{V_{OC}}{R_P} \right) \frac{\left[\exp \left(\frac{qV_{OC}}{akN_C T} \right) - 1 \right]}{\exp \left(\frac{qV_{OC}}{akN_C T} \right) - \exp \left(\frac{qR_S I_{SC}}{akN_C T} \right)} + \frac{V_{OC}}{R_P} \text{ (Biswas et al., 2018)}$$

- **Current at maximum power point (I_{MPP})**

$$I_{MPP} = I_{PV} - I_O \left[\exp \frac{q(V_{MPP}+R_S I_{MPP})}{akN_C T} - 1 \right] - \frac{V_{MPP}+R_S I_{MPP}}{R_P} \text{ (Biswas et al., 2018)}$$

In keeping with our concept of mathematical modeling, the double-diode model takes into consideration recombination losses within the depletion region, providing a more accurate depiction of PV module performance. According to Biswas et al., the I-V characteristic equation for a PV module's double-diode model is as follows:

$$I = I_{PV} - I_{O1} \left[\exp \frac{q(V+R_S I)}{a_1 k N_C T} - 1 \right] - I_{O2} \left[\exp \frac{q(V+R_S I)}{a_2 k N_C T} - 1 \right] - \frac{V+R_S I}{R_P} \text{ (Biswas et al., 2018)}$$

The reverse saturation currents of the two diodes are denoted by I_{O1} and I_{O2} in this equation, while the ideality factors for each are denoted by a_1 and a_2 .

An objective function is usually developed for parameter estimation in order to reduce the difference between the model's predictions and the measured data. According to Biswas et al. (Biswas et al., 2018), the goal of optimization is to minimize mistakes at the maximum power points, open circuit, and short circuit. The sum of the squared errors at these three crucial operational points is the aggregate error (ERR) that is employed in their objective function:

$$ERR = err_{OC}^2 + err_{SC}^2 + err_{MPP}^2 \text{ (Biswas et al., 2018)}$$

The current-voltage relationships at the open circuit, short circuit, and maximum power points are used to derive these individual error values (err_{OC} , err_{SC} , err_{MPP}) for the double-diode model in a manner similar to that of the single-diode model, specifically referring to equations and the paper (Biswas et al., 2018). At these critical locations, the goal of this optimization is to properly estimate the PV cell parameters so that the I-V characteristics of the model match the actual data (Biswas et al., 2018).

Numerical Data

Our research leveraged comprehensive numerical data for three distinct types of solar cell modules: polycrystalline, monocrystalline, and thin-film, consistent with the module types often characterized in the literature Biswas et al. (2018) . This typical manufacturer-provided data included current and voltage values at the short circuit, open circuit, and maximum power points. All data was acquired under standard test conditions, specifically 25°C and 1000 W/m² irradiance. As shown in Table 2.

This analysis is crucial for optimizing solar power generation in varied environmental conditions Chakraborty et al. (2023) Lin and Yu (2025).

5. Application and Validation

Power Output Prediction

By understanding the potential power output, grid operators can make informed decisions about energy dispatch and grid stability Xuan et al. (2024). This facilitates more effective grid management and energy trading strategies Paulescu and Paulescu (2019). It also aids in minimizing the forecasting errors by choosing suitable models and preprocessing methods Robrini et al. (2025) Teixeira et al. (2024). This can lead to improved energy independence and reduced carbon footprints Kalra et al. (2024) T et al. (2024).

6. Case Studies

Japanese Power Utility Case Studies

Japanese electric power companies are actively engaged in promoting renewable energy, aligning with national goals to make renewables a primary power source. Their strategies involve significant investments, organizational restructuring, and adaptation to new market mechanisms.

6.1. Electric Utility Landscape and Market Share

The Japanese power market is primarily dominated by former General Electricity Utilities (10 EPCOs from Hokkaido to Okinawa), which held 81.9% of the market share based on electricity demand in December 2022. Power Producers and Suppliers accounted for the remaining 18.1% Yamazaki and Ikki (2022).

6.2. Renewable Energy Development Targets and Initiatives

Many electric companies have established ambitious targets for renewable energy development and are undergoing internal reorganization to facilitate these goals Yamazaki and Ikki (2022):

The Federation of Electric Power Companies also announced plans to construct large-scale PV power plants with a total capacity of 140 MW, with construction almost completed Yamazaki and Ikki (2022).

6.3. Grid Integration and Challenges

With the expansion of PV installations, challenges related to grid integration have emerged, particularly concerning output curtailment and grid connection:

Yamazaki2022

- **Output Curtailment:** Output curtailment of renewable energy has been conducted, initially in Kyushu in October 2018, and expanded to Hokkaido, Tohoku, Chugoku, and Shikoku areas in 2022. This occurs on weekends and now weekdays due to increased PV penetration Yamazaki and Ikki (2022). The Organization for Cross-regional Coordination of Transmission Operators, JAPAN, verifies the appropriateness of this curtailment Yamazaki and Ikki (2022).
- **Grid Connection Policies:** Some electric companies temporarily suspended responses to new grid connection applications in 2014 due to the growth of PV capacity. They then introduced a limit of 30 days/year or 360 hours/year for output curtailment to manage grid capacity Yamazaki and Ikki (2022).
- **Grid Enhancement:** Efforts are underway to enhance inter-regional grid connection lines to transport electricity from areas with abundant renewable energy resources to demand centers. This includes frequency conversion stations and a master plan for wide-area interconnection systems Yamazaki and Ikki (2022). A new wheeling scheme, the "revenue cap system," is scheduled for introduction in FY 2023, which is expected to increase wheeling charges in various regions Yamazaki and Ikki (2022).

6.4. New Business Models and Partnerships

Electric companies are also adapting to new business models to integrate more renewable energy:

- **Corporate Power Purchase Agreements:** Both on-site and off-site Corporate PPA schemes are progressing, targeting electricity users and large customers, driven by rising electricity bills Yamazaki and Ikki (2022).
- **Self-Consumption:** Electric companies are advancing activities to promote self-consumption of PV electricity, especially for residential PV systems whose Feed-in Tariff purchase period has terminated Yamazaki and Ikki (2022).
- **Surplus Electricity Purchase:** Electric companies and Power Producers and Suppliers offer purchase menus for surplus electricity from post-FIT residential PV systems Yamazaki and Ikki (2022)

These points highlight the significant role Japanese power utilities play in the country's renewable energy transition, addressing both technical and market-related challenges.

Table 2: Electrical parameters for the PV cells at standard test conditions (STC).

| Parameter | KC200GT (K.C. (2004)) | SQ85 (Soon et al. (2012)) | ST40 (Soon et al. (2012)) |
|---|-----------------------|---------------------------|---------------------------|
| Type | Polycrystalline | Monocrystalline | Thin film |
| Open circuit voltage, V_{OC} (volt) | 32.9 | 22.20 | 23.30 |
| Short circuit current, I_{SC} (amp) | 8.21 | 5.45 | 2.68 |
| Voltage at maximum power, V_{MPP} (volt) | 26.3 | 17.20 | 16.60 |
| Current at maximum power, I_{MPP} (amp) | 7.61 | 4.95 | 2.41 |
| Temperature coefficient of V_{OC} , $K_{V,OC}$ (volt/ $^{\circ}$ C) | -0.123 | -0.0725 | -0.1 |
| Temperature coefficient of I_{SC} , $K_{I,SC}$ (amp/ $^{\circ}$ C) | 3.18×10^{-3} | 0.8×10^{-3} | 0.35×10^{-3} |
| Number of cells in series, N_C | 54 | 36 | 36 |

Table 3: Renewable Energy Targets by Japanese Electric Utilities

| Utility | Renewable Energy Target | Notes |
|-------------------------|---|---|
| Hokkaido Electric Power | >300 MW increase in renewable energy capacity in Hokkaido and other regions by 2030; carbon neutral by 2050 | Established Renewable Energy Development Promotion Department (Yamazaki and Ikki, 2022) |
| Tohoku Electric | 2 GW renewable energy target as early as 2030 onwards | Established Corporate PPA Office (Yamazaki and Ikki, 2022) |
| Chubu Electric | >3.2 GW renewable energy development by 2030 | Formulated "Chubu Electric Power Group Management Vision 2.0" (Yamazaki and Ikki, 2022) |
| Hokuriku Electric | Accelerate renewable energy development to achieve "Hokuriku Electric Power Group 2030 Long-term Vision" | Established Renewable Energy Department (Yamazaki and Ikki, 2022) |
| Kansai Electric Power | Invest 340 BJPY in renewable energy-related projects | Formulated "Kansai Electric Power Group Medium-term Management Plan (2021–2025)" (Yamazaki and Ikki, 2022) |
| Chugoku Electric | 300 to 700 MW renewable energy by FY 2030; carbon neutrality by 2050 | Under group management vision "Energia Change 2030" (Yamazaki and Ikki, 2022) |
| Shikoku Electric | 500 MW by FY 2030 and 2 GW by FY 2050; carbon neutrality by 2050 | Focusing on new development of renewable energy (Yamazaki and Ikki, 2022) |
| Okinawa Electric | Invest about 6 BJPY by FY 2025 | Increase installed capacity of renewable energy and upgrade grid stabilization technology using storage batteries (Yamazaki and Ikki, 2022) |
| TEPCO Renewable Power | Succeeded approximately 10 GW of renewable energy power sources; aims to develop 6–7 GW by mid-2030s | Includes hydro, wind, and PV projects in Japan and abroad (Yamazaki and Ikki, 2022) |

7. Discussion

The method combines analytical and metaheuristic approaches to optimize parameters for both single- and double-diode models, ensuring all PV cell parameters are optimized without presumptions Biswas et al. (2018). This enhances the accuracy of PV system simulations, especially in environments with limited data Biswas et al. (2018).

This is accomplished by reducing the discrepancy between the PV system's simulated and experimental I-V data Biswas et al. (2018). Additionally, this makes it easier to design and manage both independent and grid-connected PV systems Biswas et al. (2018). This method provides a workable solution for performance prediction and optimization, and is especially beneficial in situations where comprehensive experimental data is not available Biswas et al. (2018). These techniques can of-

fer more dependable and economical grid integration of solar electricity (Guo et al., 2020) (Ascencio-Vázquez et al., 2020). Ultimately, the created model boosts the financial return of solar installations both on and off the grid by providing a simplified method for improving energy output estimations and fine-tuning inverter designs (Guo et al., 2020) (Khan et al., 2021).

To validate our models and present our findings, we generated several tables and figures within our study, mirroring the comprehensive reporting standards found in Biswas et al. (2018):

8. Results

All experiments were conducted on AMD Ryzen 7 7730U with Radeon Graphics (2.00 GHz) with 16.0 GB RAM (13.8 GB usable) running 64-bit operating system.

8.1. Parameter Estimation Results

All three algorithms successfully extracted PV parameters satisfying I-V relationships at three critical operating points. Key findings include photovoltaic currents that aligned with theoretical expectations: KC200GT (8.21–8.37 A), Shell SQ85 (5.45–5.56 A), and Shell ST40 (2.68–2.73 A). Series resistance optimization frequently achieved $R_s = 0.0010 \Omega$ boundary constraint, and multiple optimal solutions were confirmed for each material, validating theoretical assertions about solution non-uniqueness. Material-specific performance analysis revealed that KC200GT (polycrystalline) exhibited the highest current generation capacity with consistent optimization across algorithms, Shell SQ85 (monocrystalline) demonstrated intermediate performance characteristics, while Shell ST40 (thin-film) showed the lowest current generation with significant algorithmic performance variations.

Table 4: Statistical summary of optimization results with different algorithms

| Case no. | Algorithm | Error function (ERR) | | | | Total CPU time (sec.) |
|---------------------------------|------------------|----------------------|-----------------------|-----------------------|-----------------------|--------------------------|
| | | Best | Worst | Mean | Std. dev. | |
| KC200GT (Single-diode model) | GA | 0 | 0 | 0 | 0 | 70.6 |
| | PSO | 0 | 0 | 0 | 0 | 18.1 |
| | ABC | 0 | 5.61×10^{11} | 4.73×10^{12} | 1.19×10^{11} | 110.3 |
| | MSA | 0 | 0 | 0 | 0 | 50.8 |
| | GWO | 0 | 2.79×10^{11} | 5.27×10^{12} | 7.80×10^{12} | 8.2 |
| | L-SHADE | 0 | 0 | 0 | 0 | 17.9 |
| | BWR(Rao (2024)) | 0 | 0 | 0 | 0 | 2.01 |
| | BMR(Rao (2024)) | 0 | 0 | 0 | 0 | 2.16 |
| KC200GT (Double-diode model) | Jaya(Rao (2016)) | 0 | 0 | 0 | 0 | 0.79 |
| | GA | 0 | 0 | 0 | 0 | 85.5 |
| | PSO | 0 | 0 | 0 | 0 | 21.7 |
| | ABC | 0 | 5.79×10^{11} | 4.84×10^{12} | 1.05×10^{11} | 150.7 |
| | MSA | 0 | 0 | 0 | 0 | 65.4 |
| | GWO | 0 | 9.86×10^{11} | 5.51×10^{12} | 1.82×10^{11} | 10.9 |
| | L-SHADE | 0 | 0 | 0 | 0 | 18.6 |
| | BWR(Rao (2024)) | 0 | 0 | 0 | 0 | 1.44 |
| Shell SQ85 | BMR | 2.0000 | 0.0010 | 117.3648 | 3.23×10 | 0 |
| | JAYA | 2.0000 | 0.0010 | 117.3639 | 3.23×10 | 0.21 |
| | BWR | 1.5570 | 0.0010 | 50.0000 | 1.01×10 | 0 |
| Shell ST40 | BMR | 1.8161 | 0.0853 | 61.5221 | 2.33×10 | 0 |
| | JAYA | 2.0000 | 0.3740 | 101.2313 | 8.33×10 | 0.05 |
| | BWR | 0.7823 | 0.2835 | 61.3265 | 2.39×10^1 | 0 |

Table 5: Optimized parameters for single-diode model using BWR, BMR, and JAYA algorithms

| Material | Algorithm | a | $R_s (\Omega)$ | $R_p (\Omega)$ | I_o (A) | I_{pv} (A) | ERR (mean) | CPU (s) |
|------------|-----------|--------|----------------|----------------|--------------------|--------------|------------|---------|
| KC200GT | BWR | 1.0273 | 0.0010 | 50.0000 | 7.13×10^1 | 8.2102 | 0 | 2.01 |
| KC200GT | BMR | 1.0273 | 0.0010 | 50.0000 | 7.13×10^1 | 8.2102 | 0 | 2.16 |
| KC200GT | JAYA | 1.0273 | 0.0010 | 50.0000 | 7.13×10^1 | 8.2102 | 0 | 0.79 |
| Shell SQ85 | BWR | 1.5570 | 0.0010 | 50.0000 | 1.01×10 | 5.4501 | 0 | 2.14 |
| Shell SQ85 | BMR | 2.0000 | 0.0010 | 117.3648 | 3.23×10 | 5.4500 | 0 | 2.16 |
| Shell SQ85 | JAYA | 2.0000 | 0.0010 | 117.3639 | 3.23×10 | 5.4500 | 0 | 0.21 |
| Shell ST40 | BWR | 0.7823 | 0.2835 | 61.3265 | 2.39×10^1 | 2.6924 | 0 | 0.88 |
| Shell ST40 | BMR | 1.8161 | 0.0853 | 61.5221 | 2.33×10 | 2.7336 | 0 | 0.05 |
| Shell ST40 | JAYA | 2.0000 | 0.3740 | 101.2313 | 8.33×10 | 2.6899 | 0 | 1.46 |

Table 6: Optimized parameters for double-diode model using BWR, BMR, and JAYA algorithms

| Material | Algorithm | a_1 | a_2 | R_s (Ω) | R_p (Ω) | I_{o1} (A) | I_{o2} (A) | I_{pv} (A) | ERR (mean) | CPU (s) |
|-----------------|------------------|-------------------------|-------------------------|---|---|--|--|--|-----------------------|--------------------|
| KC200GT | BWR | 1.2784 | 1.0344 | 0.2192 | 74.9367 | 8.05×10^{-12} | 8.05×10^{-11} | 8.3742 | 0 | 1.44 |
| KC200GT | BMR | 1.0442 | 0.7540 | 0.0024 | 50.0166 | 9.41×10^{-10} | 9.41×10^{-9} | 8.3742 | 0 | 3.58 |
| KC200GT | JAYA | 1.0911 | 0.5008 | 0.0510 | 50.0146 | 1.64×10^{-9} | 1.64×10^{-8} | 8.3742 | 0 | 1.37 |
| Shell SQ85 | BWR | 1.9181 | 1.5487 | 0.0082 | 50.1358 | 1.30×10^{-9} | 1.30×10^{-8} | 5.5590 | 0 | 3.36 |
| Shell SQ85 | BMR | 1.2354 | 0.7562 | 0.5196 | 50.1373 | 1.95×10^{-10} | 1.95×10^{-9} | 5.5590 | 0 | 3.49 |
| Shell SQ85 | JAYA | 1.9625 | 1.9985 | 0.0013 | 116.9369 | 4.60×10^{-8} | 4.60×10^{-7} | 5.5590 | 0 | 0.35 |
| Shell ST40 | BWR | 1.3204 | 1.2444 | 0.6085 | 67.1851 | 6.46×10^{-10} | 6.46×10^{-9} | 2.7336 | 0 | 3.18 |
| Shell ST40 | BMR | 1.7336 | 0.7306 | 0.2492 | 61.2966 | 1.10×10^{-10} | 1.10×10^{-9} | 2.7336 | 0 | 3.43 |
| Shell ST40 | JAYA | 1.9288 | 1.9906 | 0.0015 | 80.1476 | 1.10×10^{-8} | 1.10×10^{-7} | 2.7336 | 0 | 0.07 |

4

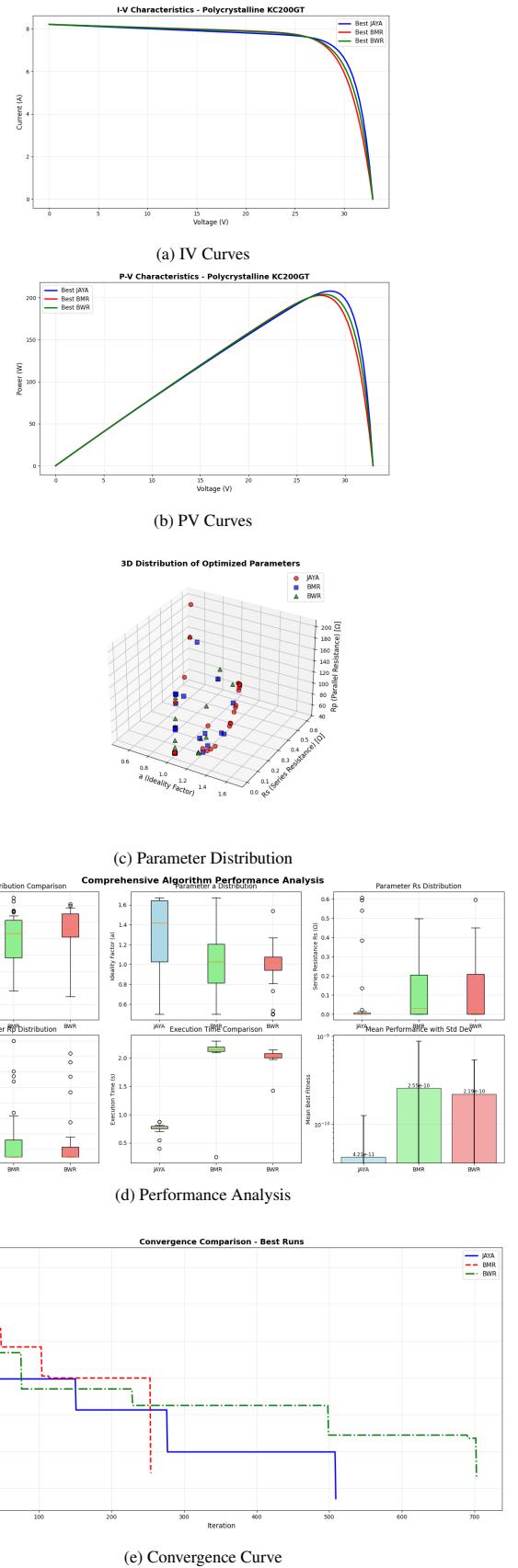
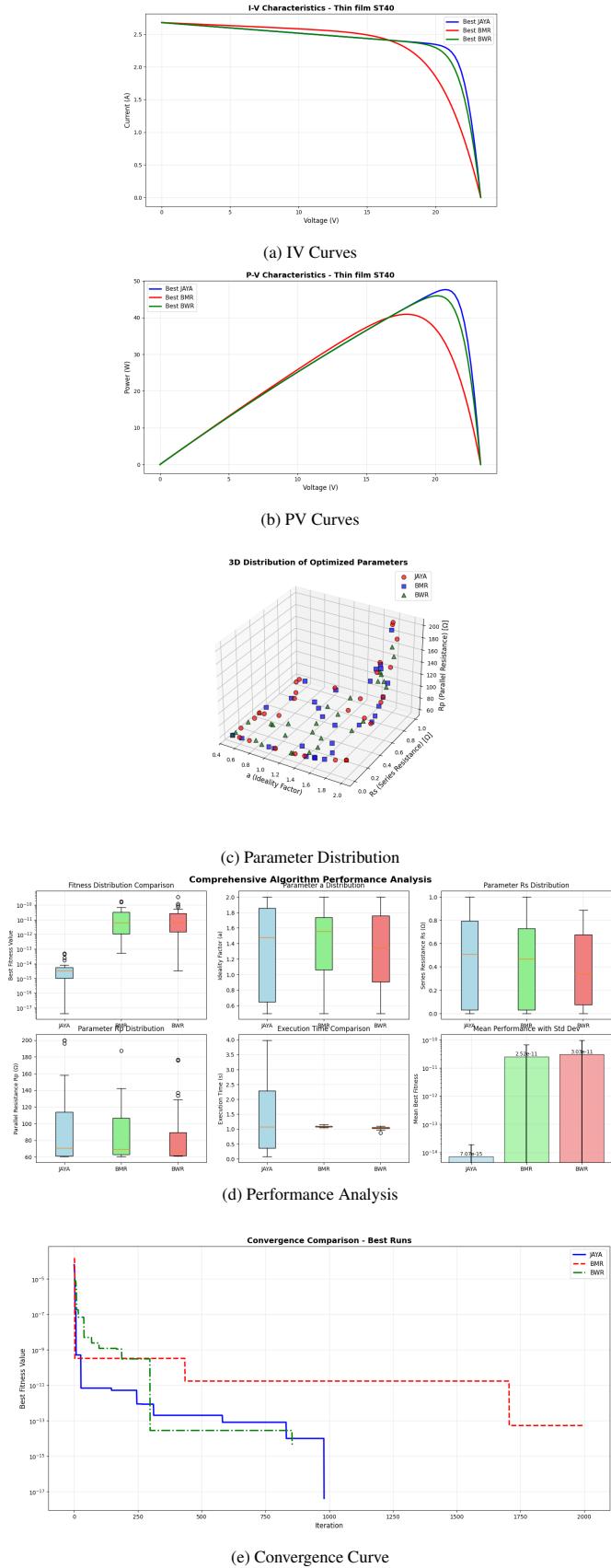
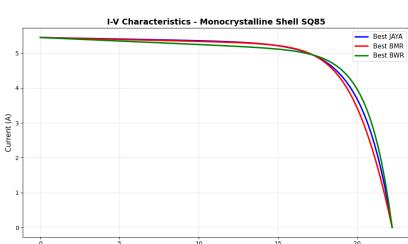
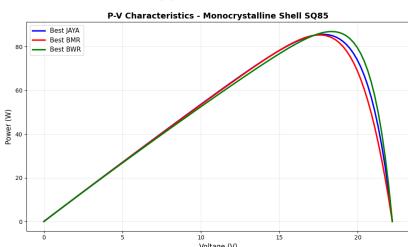


Figure 1: Graphical Visualization of Single-Diode (Shell ST40) Behavior Using BWR, BMR and JAYA Optimization Algorithm

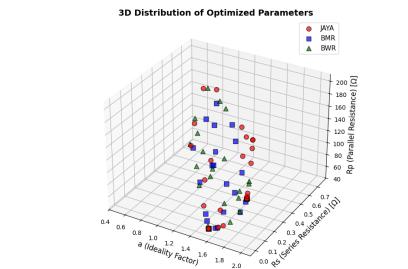
Figure 2: Graphical Visualization of Single-Diode (KC400GT) Behavior Using BWR, BMR and JAYA Optimization Algorithm



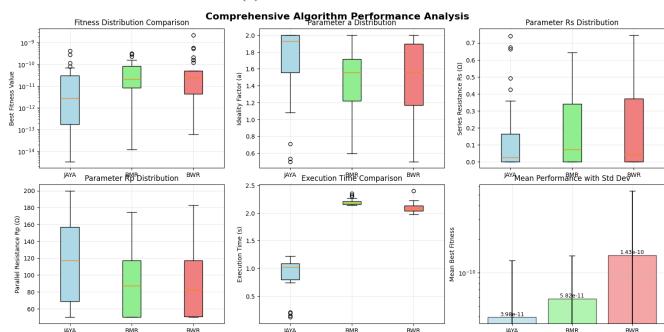
(a) IV Curves



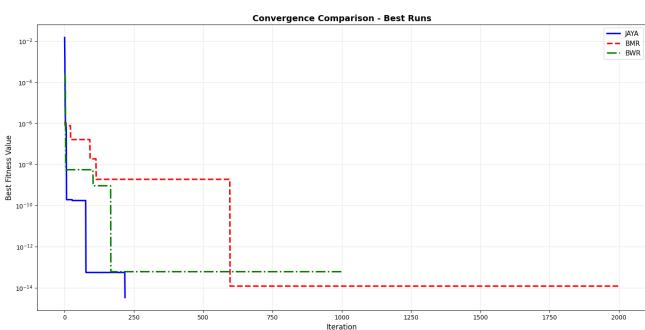
(b) PV Curves



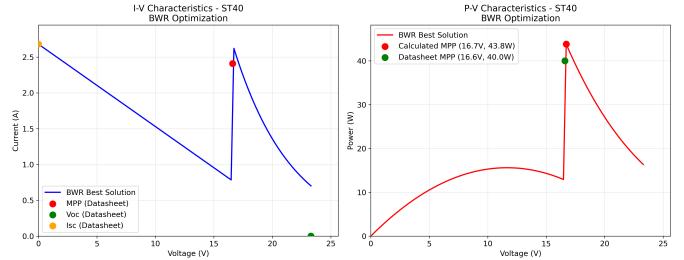
(c) Parameter Distribution



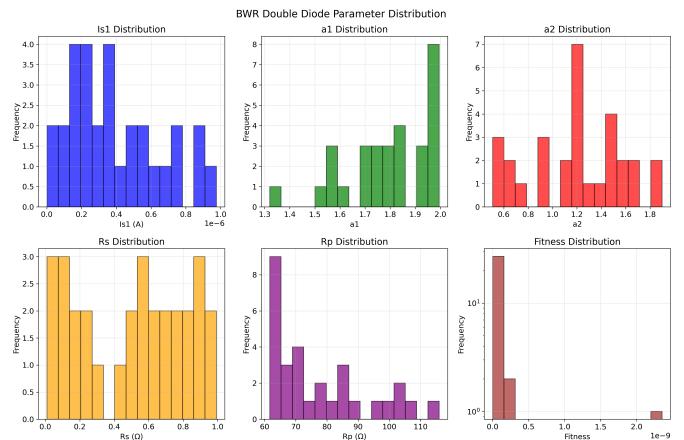
(d) Performance Analysis



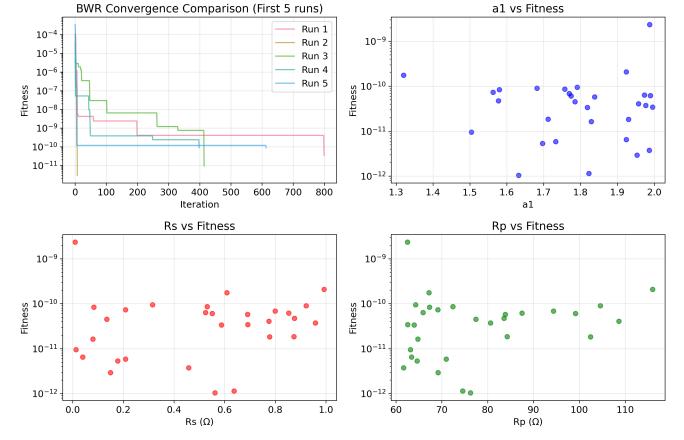
(e) Convergence Curve



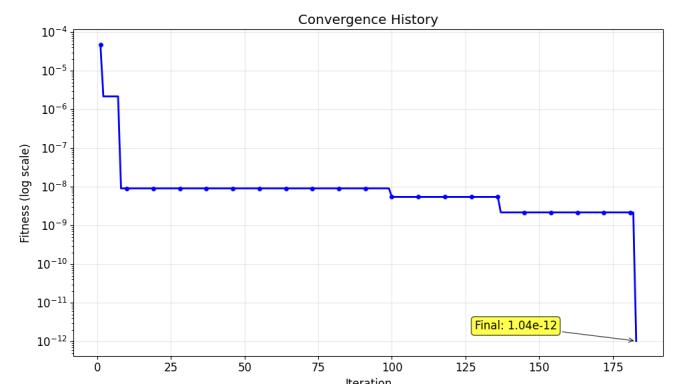
(a) IV and PV Curves



(b) Parameter Distribution



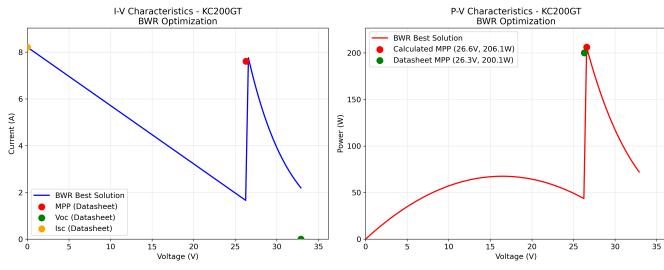
(c) Statistical Analysis



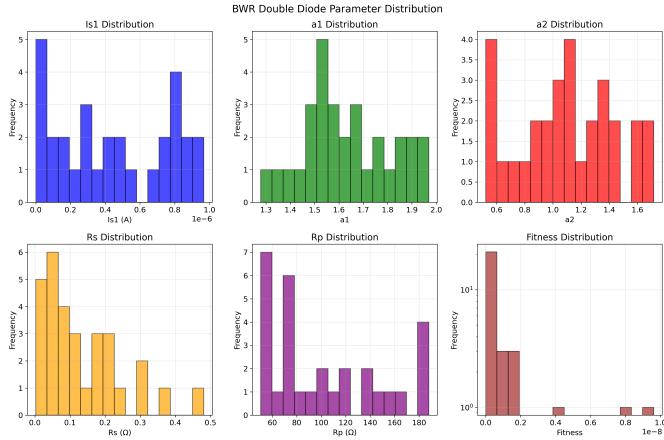
(d) BWR Shell ST40

Figure 3: Graphical Visualization of Single-Diode (Shell SQ85) Behavior Using BWR, BMR and JAYA Optimization Algorithm

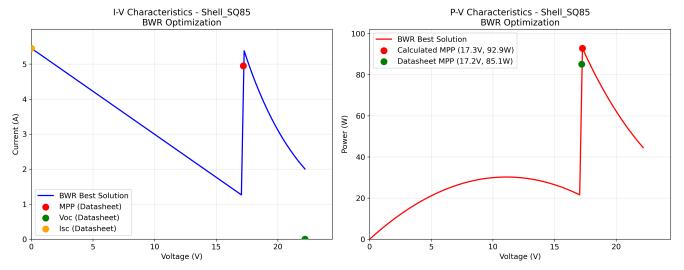
Figure 4: Graphical Visualization of Double-Diode (Shell ST40) Behavior Using BWR Optimization Algorithm



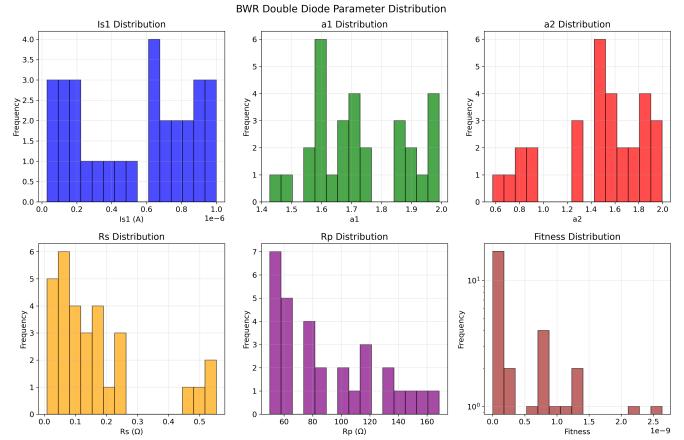
(a) IV and PV Curves



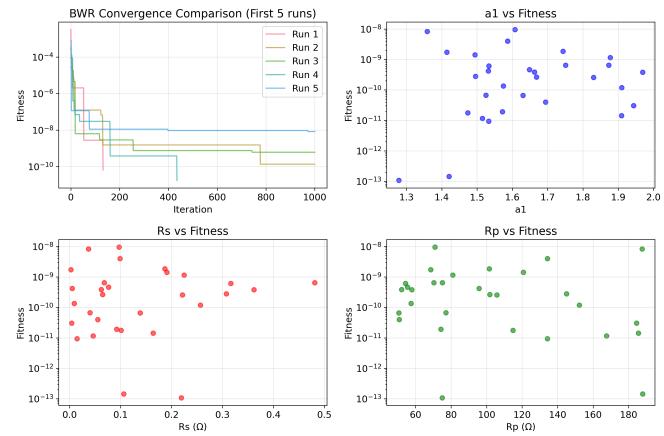
(b) Parameter Distribution



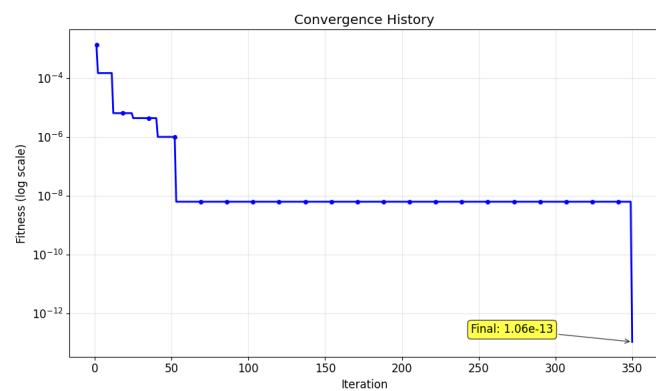
(a) IV and PV Curves



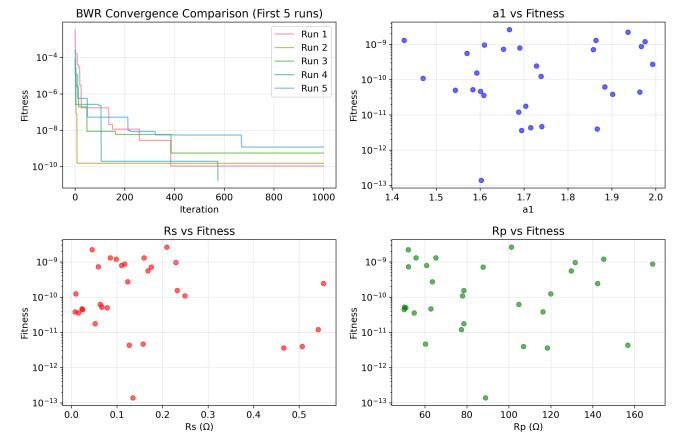
(b) Parameter Distribution



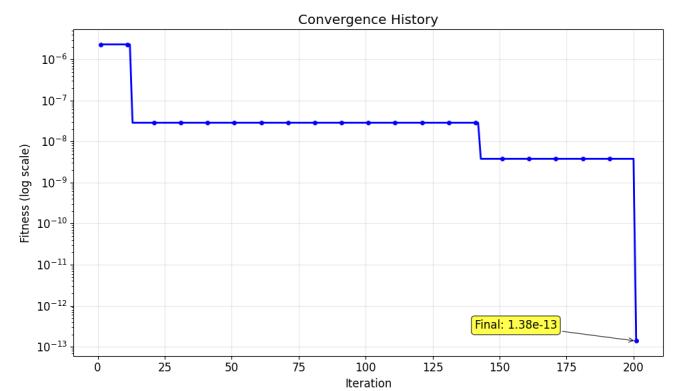
(c) Statistical Analysis



(d) BWR KC200GT



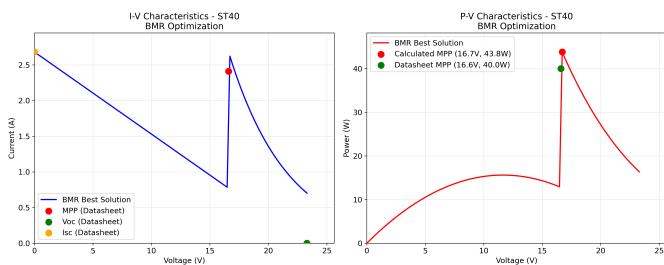
(c) Statistical Analysis



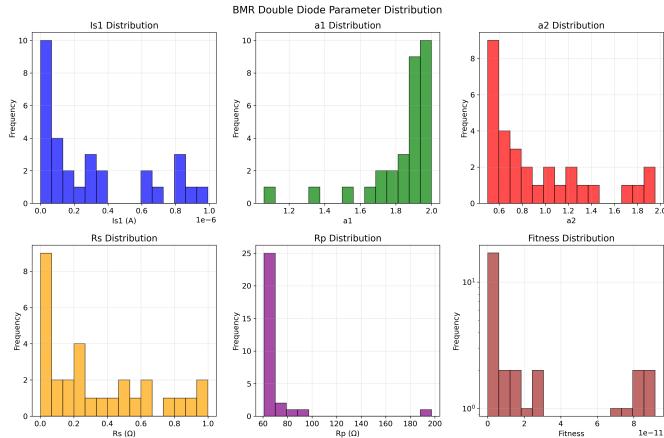
(d) BWR Shell SQ85

Figure 5: Graphical Visualization of Double-Diode (KC200GT) Behavior Using BWR Optimization Algorithm

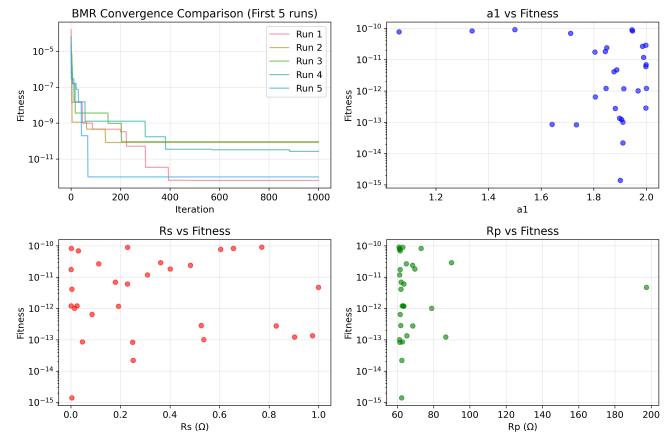
Figure 6: Graphical Visualization of Double-Diode (Shell SQ85) Behavior Using BWR Optimization Algorithm



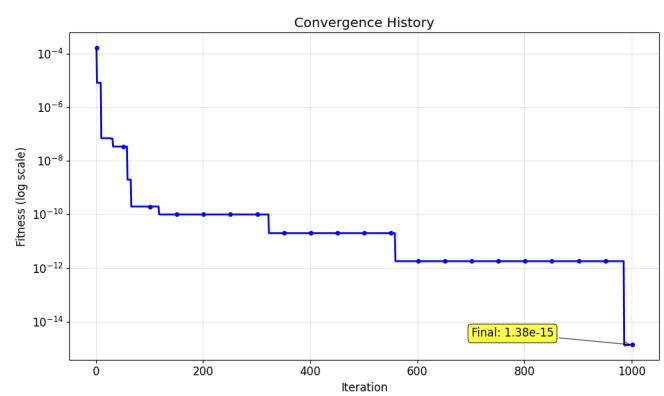
(a) IV and PV Curves



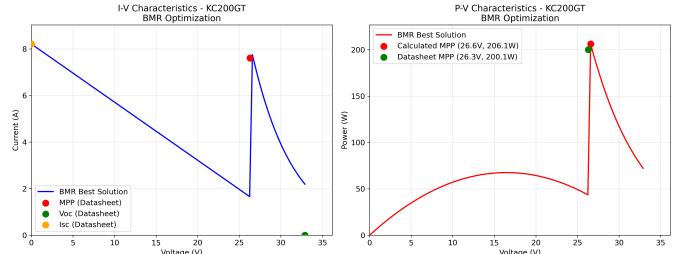
(b) Parameter Distribution



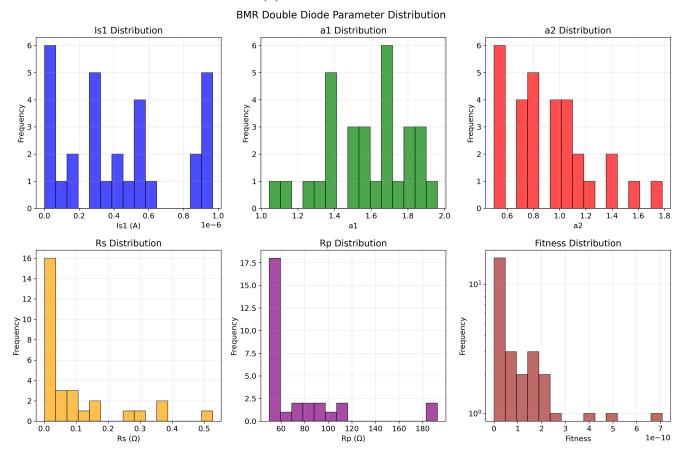
(c) Statistical Analysis



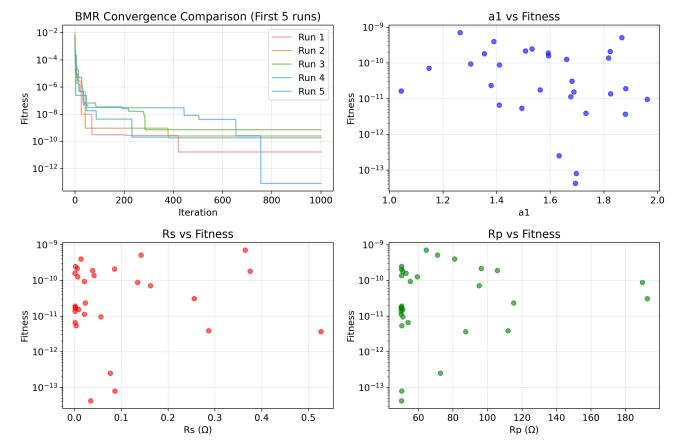
(d) BMR Shell ST40



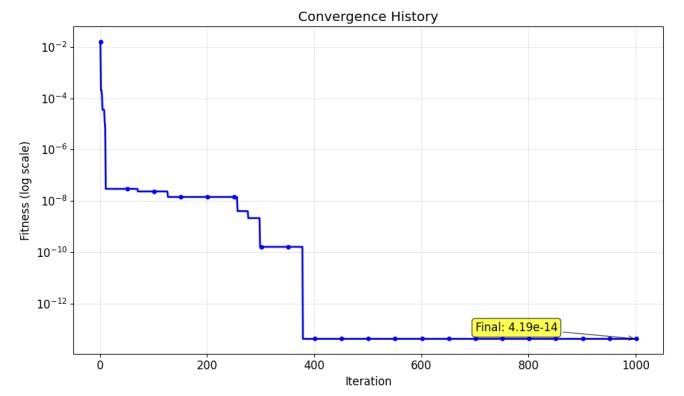
(a) IV and PV Curves



(b) Parameter Distribution



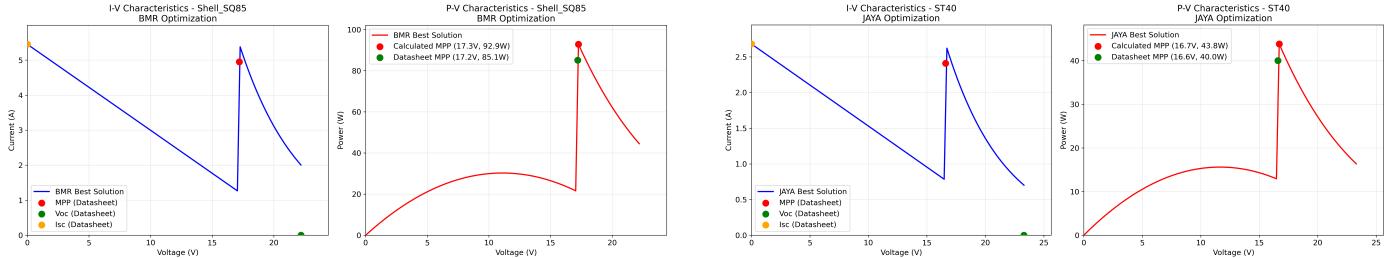
(c) Statistical Analysis



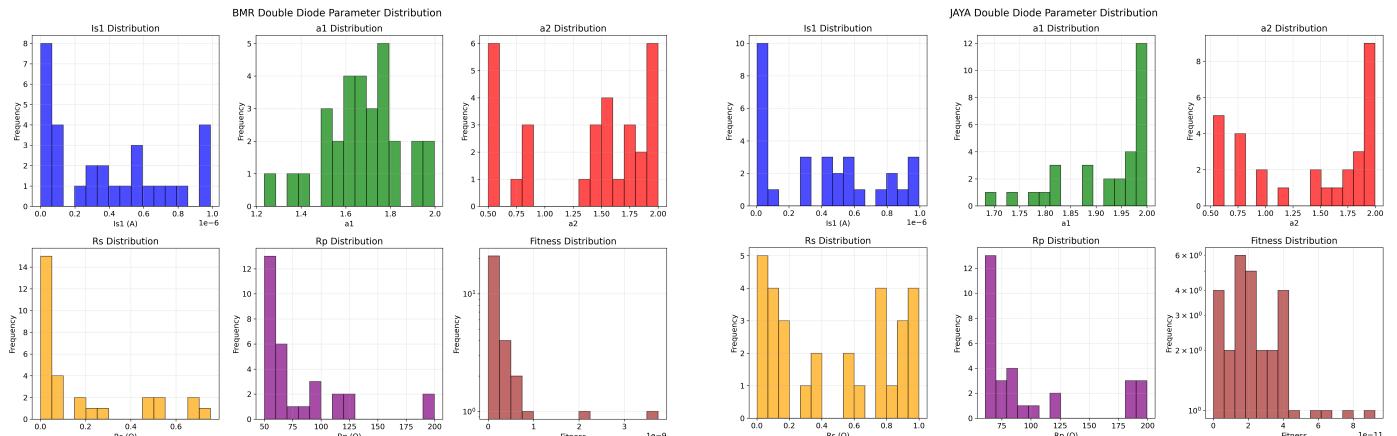
(d) BMR KC400GT

Figure 7: Graphical Visualization of Double-Diode (Shell ST40) Behavior Using BMR Optimization Algorithm

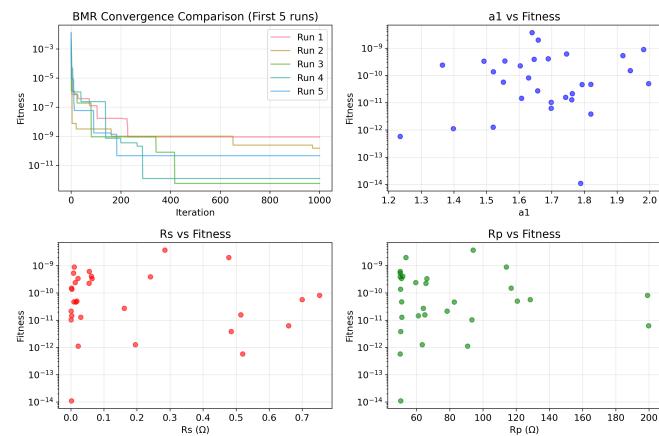
Figure 8: Graphical Visualization of Double-Diode (KC200GT) Behavior Using BMR Optimization Algorithm



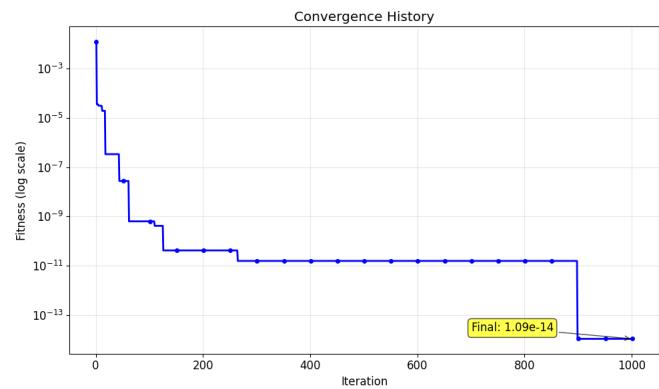
(a) IV and PV Curves



(b) Parameter Distribution

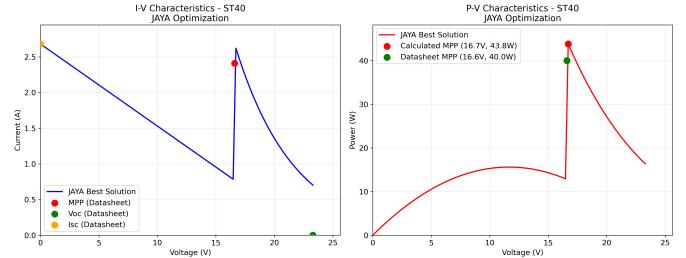


(c) Statistical Analysis

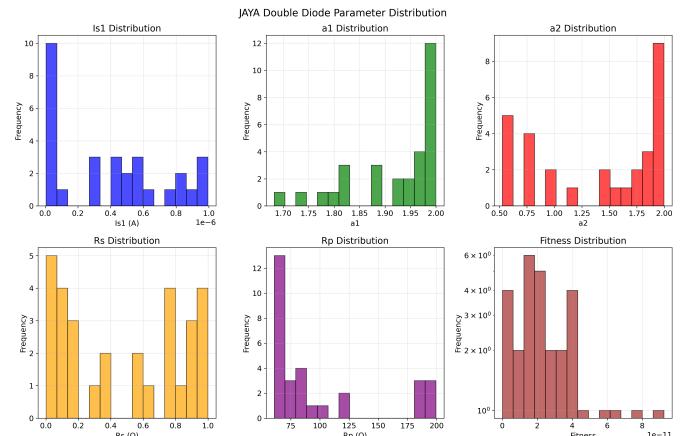


(d) BMR Shell SQ85

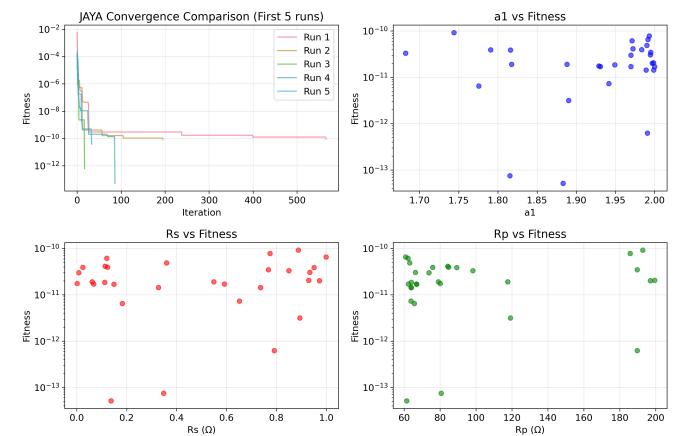
Figure 9: Graphical Visualization of Double-Diode (Shell SQ85) Behavior Using BMR Optimization Algorithm



(a) IV and PV Curves



(b) Parameter Distribution



(c) Statistical Analysis

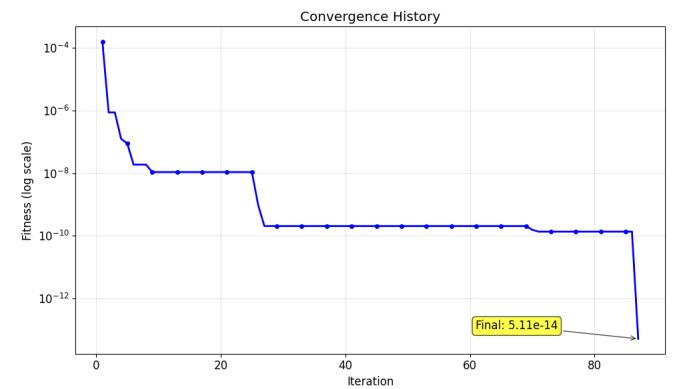
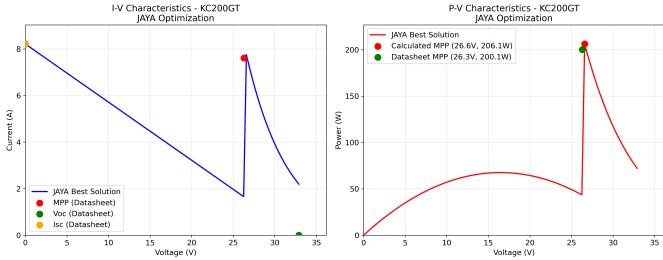
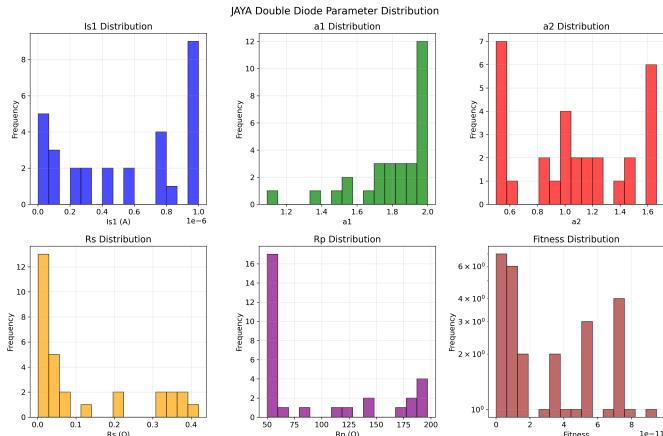


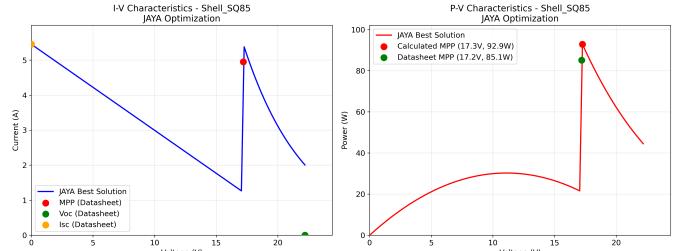
Figure 10: Graphical Visualization of Double-Diode (Shell ST40) Behavior Using JAYA Optimization Algorithm



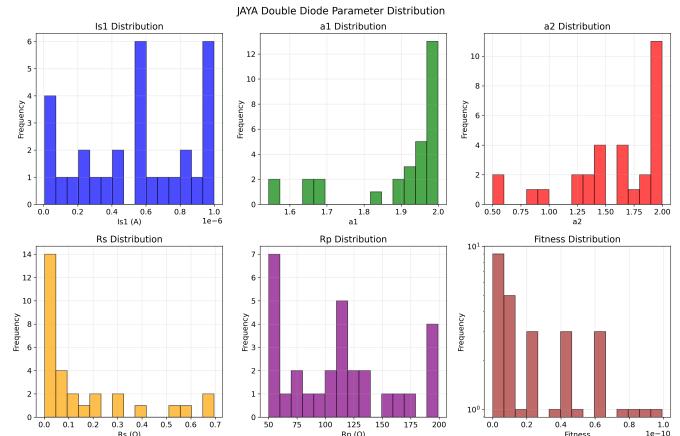
(a) IV and PV Curves



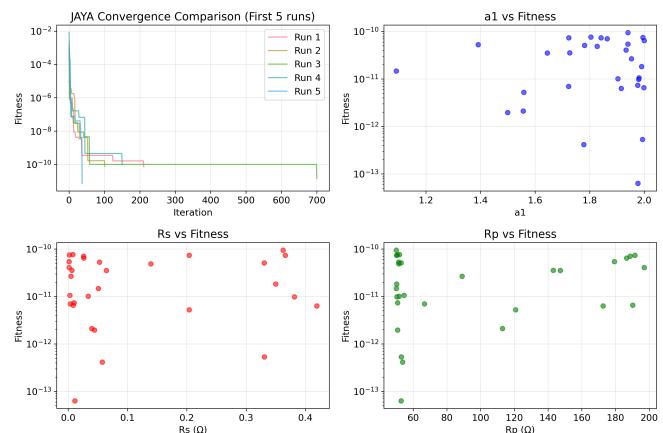
(b) Parameter Distribution



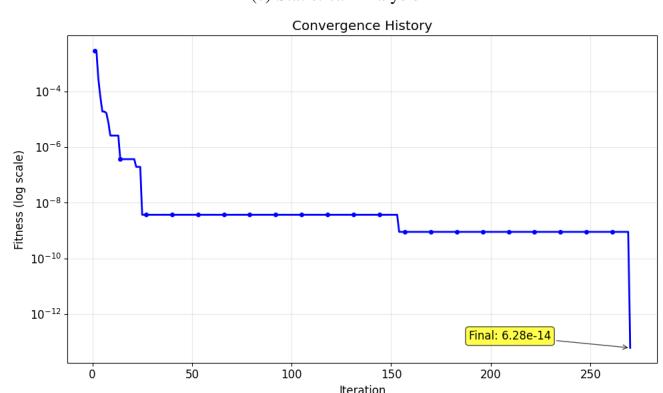
(a) IV and PV Curves



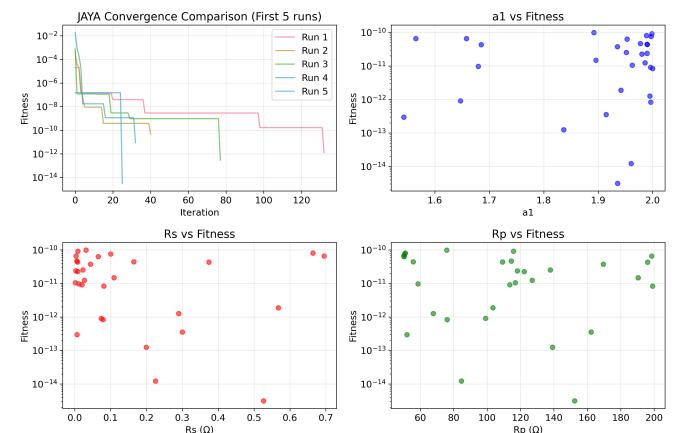
(b) Parameter Distribution



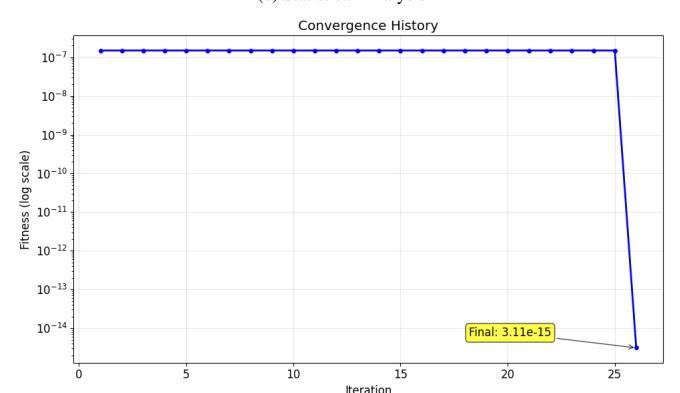
(c) Statistical Analysis



(d) JAYA KC400GT



(c) Statistical Analysis



(d) JAYA Shell SQ85

Figure 11: Graphical Visualization of Double-Diode (KC400GT) Behavior Using JAYA Optimization Algorithm

Figure 12: Graphical Visualization of Double-Diode (Shell SQ85) Behavior Using JAYA Optimization Algorithm

9. Conclusion

This study successfully validates three metaheuristic algorithms (BWR, BMR, JAYA) for PV parameter estimation using limited datasheet information. JAYA algorithm emerges as the most computationally efficient solution, achieving convergence up to 20 times faster than competing methods while maintaining solution quality.

The research confirms that multiple parameter sets can satisfy datasheet constraints, providing design flexibility but requiring careful parameter selection based on application needs. All algorithms demonstrated reliable parameter extraction capabilities, supporting accurate PV modeling for grid integration and energy forecasting applications.

The demonstrated computational efficiency makes these methods suitable for real-time applications in Japan's smart grid infrastructure, directly supporting the nation's 120 GW PV capacity target by 2030 through enhanced system modeling and operational planning capabilities.

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A. BWR Algorithm

A.1. Single-Diode Model

A.1.1. Shell ST40 (Thin-Film)

Table A.7: Optimal parameters for single-diode model of *Shell ST40* using BWR.

| Run | a | R_s (Ω) | R_p (Ω) | I_0 (A) | I_{pv} (A) | ERR | Time(s) |
|-----|--------|-----------|-----------|-----------|--------------|-----|---------|
| 1 | 2.0000 | 0.0010 | 80.5745 | 8.10e-06 | 2.6800 | 0 | 1.04 |
| 2 | 0.5000 | 0.0453 | 61.4372 | 3.03e-22 | 2.6820 | 0 | 1.03 |
| 3 | 1.1652 | 0.6974 | 66.2752 | 9.62e-10 | 2.7082 | 0 | 1.02 |
| 4 | 1.7390 | 0.8162 | 118.6287 | 1.28e-06 | 2.6984 | 0 | 1.07 |
| 5 | 1.3734 | 0.8168 | 77.2805 | 2.60e-08 | 2.7083 | 0 | 1.06 |
| 6 | 0.7934 | 0.0279 | 61.5178 | 3.74e-14 | 2.6812 | 0 | 1.07 |
| 7 | 1.2901 | 0.0010 | 63.4647 | 7.65e-09 | 2.6800 | 0 | 1.05 |
| 8 | 1.5205 | 0.1357 | 67.6611 | 1.49e-07 | 2.6854 | 0 | 1.09 |
| 9 | 1.0326 | 0.1976 | 62.0696 | 5.87e-11 | 2.6885 | 0 | 1.10 |
| 10 | 1.8837 | 0.8498 | 176.6673 | 3.99e-06 | 2.6929 | 0 | 1.01 |
| 11 | 0.5000 | 0.3840 | 61.0993 | 3.05e-22 | 2.6968 | 0 | 1.04 |
| 12 | 1.2876 | 0.3211 | 65.0431 | 7.44e-09 | 2.6932 | 0 | 1.04 |
| 13 | 0.5000 | 0.2220 | 61.2591 | 3.04e-22 | 2.6897 | 0 | 1.00 |
| 14 | 1.4794 | 0.0548 | 66.1225 | 9.38e-08 | 2.6822 | 0 | 1.05 |
| 15 | 1.3917 | 0.5958 | 71.4071 | 3.27e-08 | 2.7024 | 0 | 1.08 |
| 16 | 1.8457 | 0.4481 | 91.8986 | 2.88e-06 | 2.6931 | 0 | 1.05 |
| 17 | 2.0000 | 0.6144 | 137.0441 | 8.54e-06 | 2.6920 | 0 | 1.05 |
| 18 | 1.7615 | 0.8396 | 128.5384 | 1.55e-06 | 2.6975 | 0 | 1.01 |
| 19 | 0.5000 | 0.0010 | 61.4805 | 3.03e-22 | 2.6800 | 0 | 0.98 |
| 20 | 1.2316 | 0.4433 | 65.0568 | 3.07e-09 | 2.6983 | 0 | 1.01 |
| 21 | 1.3140 | 0.0010 | 63.6885 | 1.09e-08 | 2.6800 | 0 | 1.06 |
| 22 | 1.7670 | 0.3641 | 81.8104 | 1.55e-06 | 2.6919 | 0 | 1.03 |
| 23 | 1.9988 | 0.7299 | 175.8436 | 8.60e-06 | 2.6911 | 0 | 0.97 |
| 24 | 1.4567 | 0.2588 | 67.6954 | 7.25e-08 | 2.6902 | 0 | 1.05 |
| 25 | 0.7526 | 0.2893 | 61.2874 | 6.71e-15 | 2.6927 | 0 | 1.04 |
| 26 | 0.9282 | 0.3565 | 61.7137 | 3.79e-12 | 2.6955 | 0 | 1.03 |
| 27 | 1.7101 | 0.8868 | 126.3171 | 1.01e-06 | 2.6988 | 0 | 1.06 |
| 28 | 1.8943 | 0.7141 | 133.3291 | 4.23e-06 | 2.6944 | 0 | 1.06 |
| 29 | 0.7823 | 0.2835 | 61.3265 | 2.39e-14 | 2.6924 | 0 | 0.88 |
| 30 | 0.8988 | 0.0010 | 61.6467 | 1.55e-12 | 2.6800 | 0 | 1.02 |

A.1.2. KC200GT (Polycrystalline)

Table A.8: Optimal parameters for single-diode model of KC200GT using BWR.

| Run | a | R_s (Ω) | R_p (Ω) | I_0 (A) | I_{pv} (A) | ERR | Time(s) |
|-----|--------|--------------------|--------------------|-----------|--------------|-----|---------|
| 1 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 1.99 |
| 2 | 0.5000 | 0.4512 | 50.0000 | 1.93e-20 | 8.2841 | 0 | 2.00 |
| 3 | 1.0273 | 0.0010 | 50.0000 | 7.12e-10 | 8.2102 | 0 | 1.97 |
| 4 | 1.0272 | 0.0010 | 50.0000 | 7.12e-10 | 8.2102 | 0 | 2.08 |
| 5 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.00 |
| 6 | 1.0273 | 0.0010 | 50.0000 | 7.12e-10 | 8.2102 | 0 | 2.11 |
| 7 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.08 |
| 8 | 0.9850 | 0.0377 | 50.0000 | 2.65e-10 | 8.2162 | 0 | 2.12 |
| 9 | 1.0279 | 0.0010 | 50.0203 | 7.22e-10 | 8.2102 | 0 | 2.02 |
| 10 | 1.0273 | 0.0010 | 50.0000 | 7.14e-10 | 8.2102 | 0 | 2.03 |
| 11 | 0.5000 | 0.4512 | 50.0000 | 1.93e-20 | 8.2841 | 0 | 2.01 |
| 12 | 0.8080 | 0.1898 | 50.0000 | 1.36e-12 | 8.2412 | 0 | 2.06 |
| 13 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.08 |
| 14 | 1.2592 | 0.0807 | 75.6624 | 5.16e-08 | 8.2188 | 0 | 2.04 |
| 15 | 0.5330 | 0.4234 | 50.0000 | 3.62e-19 | 8.2795 | 0 | 2.07 |
| 16 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.05 |
| 17 | 0.5000 | 0.5955 | 133.4840 | 2.02e-20 | 8.2466 | 0 | 2.14 |
| 18 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.01 |
| 19 | 1.0884 | 0.2342 | 94.9272 | 2.72e-09 | 8.2303 | 0 | 2.08 |
| 20 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.06 |
| 21 | 1.2599 | 0.2045 | 172.5042 | 5.38e-08 | 8.2197 | 0 | 2.04 |
| 22 | 0.5000 | 0.4512 | 50.0000 | 1.93e-20 | 8.2841 | 0 | 2.11 |
| 23 | 1.5396 | 0.0628 | 183.9525 | 1.64e-06 | 8.2128 | 0 | 2.05 |
| 24 | 0.7328 | 0.2540 | 50.0000 | 6.72e-14 | 8.2517 | 0 | 1.97 |
| 25 | 1.2698 | 0.0010 | 62.9564 | 5.96e-08 | 8.2101 | 0 | 1.98 |
| 26 | 1.2310 | 0.2110 | 153.9184 | 3.44e-08 | 8.2213 | 0 | 2.01 |
| 27 | 1.1959 | 0.0877 | 68.4800 | 1.89e-08 | 8.2205 | 0 | 2.04 |
| 28 | 1.0274 | 0.0010 | 50.0000 | 7.14e-10 | 8.2102 | 0 | 1.97 |
| 29 | 1.2627 | 0.0065 | 63.0284 | 5.37e-08 | 8.2108 | 0 | 1.42 |
| 30 | 0.9253 | 0.0891 | 50.0000 | 5.61e-11 | 8.2246 | 0 | 2.01 |

A.1.3. Shell SQ85 (Monocrystalline)

Table A.9: Optimal parameters for single-diode model of *Shell SQ85* using BWR.

| Run | a | R_s (Ω) | R_p (Ω) | I_0 (A) | I_{pv} (A) | ERR | Time(s) |
|-----|--------|-----------|-----------|-----------|--------------|-----|---------|
| 1 | 2.0000 | 0.0010 | 117.3684 | 3.23e-05 | 5.4500 | 0 | 2.10 |
| 2 | 1.5961 | 0.1279 | 73.8150 | 1.52e-06 | 5.4594 | 0 | 2.05 |
| 3 | 2.0000 | 0.0010 | 117.3701 | 3.23e-05 | 5.4500 | 0 | 2.09 |
| 4 | 1.5243 | 0.0225 | 50.0000 | 7.27e-07 | 5.4524 | 0 | 2.00 |
| 5 | 0.6246 | 0.6689 | 76.6043 | 1.06e-16 | 5.4976 | 0 | 2.04 |
| 6 | 1.1757 | 0.4436 | 178.8766 | 7.27e-09 | 5.4635 | 0 | 2.04 |
| 7 | 1.3924 | 0.3039 | 112.9848 | 1.72e-07 | 5.4647 | 0 | 2.08 |
| 8 | 2.0000 | 0.0010 | 117.3666 | 3.23e-05 | 5.4500 | 0 | 1.98 |
| 9 | 1.8364 | 0.0637 | 102.2162 | 1.10e-05 | 5.4534 | 0 | 1.98 |
| 10 | 1.5571 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 2.00 |
| 11 | 0.8394 | 0.6035 | 168.1033 | 2.04e-12 | 5.4696 | 0 | 2.09 |
| 12 | 0.5000 | 0.6887 | 50.0000 | 7.22e-21 | 5.5251 | 0 | 2.22 |
| 13 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 2.08 |
| 14 | 0.8537 | 0.5355 | 71.9007 | 3.20e-12 | 5.4906 | 0 | 2.06 |
| 15 | 0.8259 | 0.4893 | 51.9589 | 1.21e-12 | 5.5013 | 0 | 2.04 |
| 16 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 2.09 |
| 17 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 2.10 |
| 18 | 1.8117 | 0.0010 | 71.9433 | 9.07e-06 | 5.4501 | 0 | 2.03 |
| 19 | 1.3370 | 0.3669 | 182.5335 | 8.53e-08 | 5.4610 | 0 | 2.06 |
| 20 | 1.9179 | 0.0042 | 92.7956 | 1.91e-05 | 5.4502 | 0 | 2.02 |
| 21 | 0.5000 | 0.7451 | 87.4036 | 7.45e-21 | 5.4965 | 0 | 2.19 |
| 22 | 1.0435 | 0.3365 | 50.0000 | 5.16e-10 | 5.4867 | 0 | 2.20 |
| 23 | 1.8308 | 0.0785 | 110.6654 | 1.06e-05 | 5.4539 | 0 | 2.40 |
| 24 | 2.0000 | 0.0211 | 137.5124 | 3.25e-05 | 5.4508 | 0 | 2.21 |
| 25 | 2.0000 | 0.0238 | 140.9149 | 3.25e-05 | 5.4509 | 0 | 2.06 |
| 26 | 2.0000 | 0.0010 | 117.3670 | 3.23e-05 | 5.4500 | 0 | 2.03 |
| 27 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 2.06 |
| 28 | 1.1663 | 0.3740 | 77.4148 | 6.00e-09 | 5.4763 | 0 | 2.15 |
| 29 | 1.1667 | 0.3505 | 68.1203 | 6.00e-09 | 5.4780 | 0 | 2.23 |
| 30 | 1.9908 | 0.0037 | 115.7713 | 3.05e-05 | 5.4502 | 0 | 2.14 |

A.2. Double-Diode Model

A.2.1. Shell ST40

Table A.10: Optimal parameters for double-diode model of *Shell ST40* using BWR.

| Run | a_1 | a_2 | R_s (Ω) | R_p (Ω) | I_{o1} (A) | I_{o2} (A) | I_{pv} (A) | ERR | Time (s) |
|-----|--------|--------|--------------------|--------------------|--------------|--------------|--------------|-----|----------|
| 1 | 1.9956 | 0.5265 | 0.6914 | 62.5366 | 3.76e-07 | 3.76e-06 | 2.7336 | 0 | 3.53 |
| 2 | 1.9536 | 1.5450 | 0.1489 | 69.1688 | 3.89e-07 | 3.89e-06 | 2.7336 | 0 | 0.05 |
| 3 | 1.5043 | 0.5092 | 0.0126 | 63.1526 | 4.64e-08 | 4.64e-07 | 2.7336 | 0 | 2.35 |
| 4 | 1.6820 | 1.1614 | 0.9215 | 104.5863 | 5.79e-07 | 5.79e-06 | 2.7336 | 0 | 2.18 |
| 5 | 1.7577 | 0.9141 | 0.5308 | 72.4043 | 6.81e-07 | 6.81e-06 | 2.7336 | 0 | 3.16 |
| 6 | 1.7121 | 1.1181 | 0.8736 | 84.2778 | 4.45e-07 | 4.45e-06 | 2.7336 | 0 | 1.90 |
| 7 | 1.9241 | 0.9459 | 0.0391 | 63.3849 | 6.08e-07 | 6.08e-06 | 2.7336 | 0 | 4.40 |
| 8 | 1.7747 | 1.8985 | 0.5508 | 99.1853 | 8.54e-07 | 8.54e-06 | 2.7336 | 0 | 1.46 |
| 9 | 1.9771 | 1.3038 | 0.9584 | 80.6245 | 1.71e-07 | 1.71e-06 | 2.7336 | 0 | 1.07 |
| 10 | 1.9896 | 1.4621 | 0.8529 | 87.4985 | 2.80e-07 | 2.80e-06 | 2.7336 | 0 | 1.44 |
| 11 | 1.8229 | 1.1684 | 0.6367 | 74.5547 | 7.69e-07 | 7.69e-06 | 2.7336 | 0 | 1.00 |
| 12 | 1.9866 | 0.6427 | 0.4574 | 61.6760 | 1.75e-07 | 1.75e-06 | 2.7336 | 0 | 1.29 |
| 13 | 1.7910 | 0.7678 | 0.3149 | 64.2980 | 3.57e-07 | 3.57e-06 | 2.7336 | 0 | 1.68 |
| 14 | 1.9304 | 1.6488 | 0.7771 | 102.4458 | 4.90e-07 | 4.90e-06 | 2.7336 | 0 | 1.21 |
| 15 | 1.6972 | 1.2055 | 0.1778 | 64.6116 | 1.31e-07 | 1.31e-06 | 2.7336 | 0 | 3.46 |
| 16 | 1.7695 | 1.3533 | 0.7995 | 94.3647 | 8.64e-07 | 8.64e-06 | 2.7336 | 0 | 0.79 |
| 17 | 1.5774 | 0.5816 | 0.8755 | 83.5777 | 2.00e-07 | 2.00e-06 | 2.7336 | 0 | 0.18 |
| 18 | 1.9574 | 1.6958 | 0.7748 | 108.6473 | 5.57e-07 | 5.57e-06 | 2.7336 | 0 | 0.24 |
| 19 | 1.8188 | 0.6622 | 0.5871 | 63.9767 | 2.83e-07 | 2.83e-06 | 2.7336 | 0 | 1.12 |
| 20 | 1.7850 | 1.8416 | 0.1345 | 77.4433 | 9.44e-08 | 9.44e-07 | 2.7336 | 0 | 0.01 |
| 21 | 1.9736 | 0.9026 | 0.5242 | 65.9171 | 9.76e-07 | 9.76e-06 | 2.7336 | 0 | 0.92 |
| 22 | 1.8381 | 1.5169 | 0.6902 | 83.8549 | 3.41e-07 | 3.41e-06 | 2.7336 | 0 | 0.89 |
| 23 | 1.9243 | 1.5037 | 0.9924 | 115.9786 | 7.66e-07 | 7.66e-06 | 2.7336 | 0 | 3.30 |
| 24 | 1.8292 | 1.1709 | 0.0798 | 64.7616 | 4.59e-07 | 4.59e-06 | 2.7336 | 0 | 0.73 |
| 25 | 1.9874 | 1.1010 | 0.0094 | 62.5199 | 1.62e-07 | 1.62e-06 | 2.7336 | 0 | 3.28 |
| 26 | 1.7327 | 1.5974 | 0.2081 | 70.9468 | 1.05e-07 | 1.05e-06 | 2.7336 | 0 | 1.39 |
| 27 | 1.6326 | 1.4366 | 0.5616 | 76.2561 | 2.06e-07 | 2.06e-06 | 2.7336 | 0 | 0.63 |
| 28 | 1.5801 | 1.2312 | 0.0831 | 67.3290 | 2.27e-07 | 2.27e-06 | 2.7336 | 0 | 1.23 |
| 29 | 1.3204 | 1.2444 | 0.6085 | 67.1851 | 6.46e-10 | 6.46e-09 | 2.7336 | 0 | 3.18 |
| 30 | 1.5631 | 1.2129 | 0.2083 | 69.1281 | 2.19e-07 | 2.19e-06 | 2.7336 | 0 | 0.48 |

A.2.2. KC200GT (Polycrystalline)

Table A.11: Optimal parameters for double-diode model of KC200GT using BWR.

| Run | a_1 | a_2 | R_s (Ω) | R_p (Ω) | I_{o1} (A) | I_{o2} (A) | I_{pv} (A) | ERR | Time (s) |
|-----|--------|--------|--------------------|--------------------|--------------|--------------|--------------|-----|----------|
| 1 | 1.6302 | 0.5677 | 0.1385 | 50.5678 | 4.23e-07 | 4.23e-06 | 8.3742 | 0 | 0.78 |
| 2 | 1.5745 | 1.0961 | 0.0090 | 57.4192 | 2.97e-07 | 2.97e-06 | 8.3742 | 0 | 6.80 |
| 3 | 1.5333 | 0.5221 | 0.3162 | 54.3020 | 1.35e-07 | 1.35e-06 | 8.3742 | 0 | 6.64 |
| 4 | 1.4738 | 0.6009 | 0.1010 | 114.8153 | 6.59e-07 | 6.59e-06 | 8.3742 | 0 | 3.08 |
| 5 | 1.3586 | 1.7167 | 0.0371 | 187.6331 | 7.90e-08 | 7.90e-07 | 8.3742 | 0 | 6.54 |
| 6 | 1.7508 | 1.1708 | 0.0681 | 70.2539 | 9.68e-07 | 9.68e-06 | 8.3742 | 0 | 6.80 |
| 7 | 1.9100 | 1.1359 | 0.2568 | 152.2282 | 2.74e-07 | 2.74e-06 | 8.3742 | 0 | 4.51 |
| 8 | 1.5720 | 0.9496 | 0.0924 | 74.2269 | 7.99e-07 | 7.99e-06 | 8.3742 | 0 | 3.67 |
| 9 | 1.4208 | 1.4651 | 0.1060 | 187.9472 | 5.28e-08 | 5.28e-07 | 8.3742 | 0 | 1.08 |
| 10 | 1.6077 | 0.9916 | 0.0969 | 70.8858 | 8.15e-07 | 8.15e-06 | 8.3742 | 0 | 7.89 |
| 11 | 1.7436 | 1.1316 | 0.1869 | 101.4884 | 7.68e-07 | 7.68e-06 | 8.3742 | 0 | 7.92 |
| 12 | 1.5320 | 1.4589 | 0.0051 | 95.7947 | 5.17e-07 | 5.17e-06 | 8.3742 | 0 | 7.36 |
| 13 | 1.9434 | 1.6451 | 0.0042 | 184.4511 | 8.92e-07 | 8.92e-06 | 8.3742 | 0 | 1.62 |
| 14 | 1.6487 | 0.8358 | 0.0764 | 55.4456 | 7.17e-07 | 7.17e-06 | 8.3742 | 0 | 7.38 |
| 15 | 1.6683 | 1.3471 | 0.0647 | 101.7721 | 8.33e-07 | 8.33e-06 | 8.3742 | 0 | 7.40 |
| 16 | 1.9094 | 1.3432 | 0.1639 | 185.5312 | 2.13e-07 | 2.13e-06 | 8.3742 | 0 | 2.37 |
| 17 | 1.4956 | 1.0244 | 0.3075 | 145.0292 | 3.43e-08 | 3.43e-07 | 8.3742 | 0 | 7.60 |
| 18 | 1.4142 | 1.3127 | 0.0025 | 68.5083 | 5.04e-08 | 5.04e-07 | 8.3742 | 0 | 7.11 |
| 19 | 1.6944 | 0.6433 | 0.0552 | 50.8021 | 8.86e-07 | 8.86e-06 | 8.3742 | 0 | 4.32 |
| 20 | 1.8734 | 0.5910 | 0.4812 | 75.1333 | 3.92e-07 | 3.92e-06 | 8.3742 | 0 | 6.76 |
| 21 | 1.6629 | 0.8752 | 0.0621 | 52.1706 | 4.80e-07 | 4.80e-06 | 8.3742 | 0 | 7.29 |
| 22 | 1.5249 | 1.2572 | 0.0398 | 77.0322 | 3.56e-07 | 3.56e-06 | 8.3742 | 0 | 1.32 |
| 23 | 1.8773 | 1.0507 | 0.2247 | 80.8807 | 9.02e-08 | 9.02e-07 | 8.3742 | 0 | 3.88 |
| 24 | 1.8300 | 1.0949 | 0.2214 | 105.7143 | 9.23e-07 | 9.23e-06 | 8.3742 | 0 | 4.05 |
| 25 | 1.5154 | 1.5672 | 0.0463 | 167.5364 | 2.97e-07 | 2.97e-06 | 8.3742 | 0 | 2.95 |
| 26 | 1.5328 | 1.5728 | 0.0145 | 134.2437 | 1.45e-07 | 1.45e-06 | 8.3742 | 0 | 0.08 |
| 27 | 1.4944 | 0.8703 | 0.1907 | 120.6428 | 5.02e-07 | 5.02e-06 | 8.3742 | 0 | 4.05 |
| 28 | 1.9696 | 0.7026 | 0.3617 | 57.9105 | 2.46e-08 | 2.46e-07 | 8.3742 | 0 | 4.19 |
| 29 | 1.2784 | 1.0344 | 0.2192 | 74.9367 | 8.05e-12 | 8.05e-11 | 8.3742 | 0 | 1.44 |
| 30 | 1.5868 | 1.3320 | 0.0987 | 134.2945 | 7.88e-07 | 7.88e-06 | 8.3742 | 0 | 4.07 |

A.2.3. Shell SQ85

Table A.12: Optimal parameters for double-diode model of *Shell SQ85* using BWR.

| Run | a_1 | a_2 | R_s (Ω) | R_p (Ω) | I_{o1} (A) | I_{o2} (A) | I_{pv} (A) | ERR | Time (s) |
|-----|--------|--------|--------------------|--------------------|--------------|--------------|--------------|-----|----------|
| 1 | 1.4702 | 1.3265 | 0.2492 | 77.8802 | 2.01e-07 | 2.01e-06 | 5.5590 | 0 | 3.43 |
| 2 | 1.5923 | 1.2912 | 0.2322 | 78.4853 | 6.48e-07 | 6.48e-06 | 5.5590 | 0 | 3.41 |
| 3 | 1.5701 | 1.9951 | 0.1679 | 129.7135 | 8.84e-07 | 8.84e-06 | 5.5590 | 0 | 3.43 |
| 4 | 1.7037 | 1.7714 | 0.0520 | 78.4699 | 6.19e-07 | 6.19e-06 | 5.5590 | 0 | 1.91 |
| 5 | 1.9753 | 1.8530 | 0.0984 | 145.2052 | 4.13e-07 | 4.13e-06 | 5.5590 | 0 | 3.25 |
| 6 | 1.9016 | 1.9871 | 0.0081 | 116.2622 | 7.77e-07 | 7.77e-06 | 5.5590 | 0 | 0.48 |
| 7 | 1.5434 | 0.8308 | 0.0783 | 50.8305 | 7.14e-07 | 7.14e-06 | 5.5590 | 0 | 1.05 |
| 8 | 1.7151 | 1.8363 | 0.1267 | 156.6993 | 9.33e-07 | 9.33e-06 | 5.5590 | 0 | 2.80 |
| 9 | 1.8636 | 1.5938 | 0.0853 | 65.1387 | 7.41e-07 | 7.41e-06 | 5.5590 | 0 | 3.25 |
| 10 | 1.9365 | 1.5144 | 0.0453 | 52.0322 | 4.20e-07 | 4.20e-06 | 5.5590 | 0 | 3.20 |
| 11 | 1.8840 | 1.8432 | 0.0634 | 104.7484 | 4.93e-07 | 4.93e-06 | 5.5590 | 0 | 0.57 |
| 12 | 1.9669 | 1.8435 | 0.1170 | 168.5214 | 3.15e-08 | 3.15e-07 | 5.5590 | 0 | 3.29 |
| 13 | 1.6880 | 0.7947 | 0.5416 | 77.3735 | 2.16e-07 | 2.16e-06 | 5.5590 | 0 | 1.23 |
| 14 | 1.6904 | 1.5145 | 0.1103 | 60.7270 | 2.41e-07 | 2.41e-06 | 5.5590 | 0 | 3.30 |
| 15 | 1.7391 | 1.9954 | 0.0096 | 119.9133 | 1.45e-07 | 1.45e-06 | 5.5590 | 0 | 3.29 |
| 16 | 1.7407 | 1.4374 | 0.1574 | 60.1858 | 8.40e-08 | 8.40e-07 | 5.5590 | 0 | 2.50 |
| 17 | 1.4272 | 1.2789 | 0.1595 | 55.7109 | 1.89e-07 | 1.89e-06 | 5.5590 | 0 | 3.28 |
| 18 | 1.9927 | 1.5137 | 0.1236 | 63.5184 | 9.21e-07 | 9.21e-06 | 5.5590 | 0 | 3.27 |
| 19 | 1.5836 | 0.5749 | 0.0667 | 50.1729 | 1.00e-06 | 1.00e-05 | 5.5590 | 0 | 0.90 |
| 20 | 1.6669 | 1.5469 | 0.2092 | 101.2510 | 1.23e-07 | 1.23e-06 | 5.5590 | 0 | 3.26 |
| 21 | 1.6084 | 1.6182 | 0.0152 | 54.8399 | 6.39e-07 | 6.39e-06 | 5.5590 | 0 | 2.57 |
| 22 | 1.7283 | 0.7008 | 0.5536 | 142.3127 | 9.55e-07 | 9.55e-06 | 5.5590 | 0 | 3.25 |
| 23 | 1.8578 | 1.5521 | 0.1753 | 87.6743 | 8.63e-07 | 8.63e-06 | 5.5590 | 0 | 3.36 |
| 24 | 1.6534 | 1.5025 | 0.0590 | 52.1421 | 2.87e-08 | 2.87e-07 | 5.5590 | 0 | 3.35 |
| 25 | 1.6098 | 1.5689 | 0.2293 | 131.5979 | 9.58e-08 | 9.58e-07 | 5.5590 | 0 | 3.26 |
| 26 | 1.9635 | 1.5014 | 0.0246 | 50.0615 | 9.41e-07 | 9.41e-06 | 5.5590 | 0 | 1.03 |
| 27 | 1.6010 | 1.7177 | 0.0233 | 62.7697 | 3.12e-07 | 3.12e-06 | 5.5590 | 0 | 0.48 |
| 28 | 1.6944 | 0.8590 | 0.4659 | 118.3185 | 8.64e-07 | 8.64e-06 | 5.5590 | 0 | 2.51 |
| 29 | 1.6027 | 1.6992 | 0.1349 | 88.8837 | 7.61e-07 | 7.61e-06 | 5.5590 | 0 | 0.65 |
| 30 | 1.8666 | 0.9355 | 0.5068 | 106.9141 | 6.59e-07 | 6.59e-06 | 5.5590 | 0 | 2.28 |

B. BMR Algorithm

B.1. Single-Diode Model

B.1.1. Shell ST40 (Thin-Film)

Table B.13: Optimal parameters for single-diode model of *Shell ST40* using BMR.

| Run | a | R_s (Ω) | R_p (Ω) | I_0 (A) | I_{pv} (A) | ERR | Time(s) |
|-----|--------|--------------------|--------------------|-----------|--------------|-----|---------|
| 1 | 2.0000 | 0.6344 | 142.1325 | 8.56e-06 | 2.6920 | 0 | 1.07 |
| 2 | 1.2207 | 0.5497 | 65.8367 | 2.56e-09 | 2.7024 | 0 | 1.07 |
| 3 | 1.4716 | 0.4487 | 71.0834 | 8.71e-08 | 2.6969 | 0 | 1.12 |
| 4 | 1.0725 | 0.6588 | 64.0354 | 1.48e-10 | 2.7076 | 0 | 1.07 |
| 5 | 1.6959 | 0.9149 | 129.1790 | 8.91e-07 | 2.6990 | 0 | 1.11 |
| 6 | 0.6234 | 0.0010 | 61.4853 | 6.49e-18 | 2.6800 | 0 | 1.09 |
| 7 | 1.7548 | 1.0000 | 187.2554 | 1.50e-06 | 2.6943 | 0 | 1.15 |
| 8 | 1.0594 | 0.9521 | 67.1041 | 1.12e-10 | 2.7180 | 0 | 1.14 |
| 9 | 2.0000 | 0.5630 | 126.0796 | 8.49e-06 | 2.6920 | 0 | 1.09 |
| 10 | 0.5000 | 0.4831 | 61.0022 | 3.05e-22 | 2.7012 | 0 | 1.06 |
| 11 | 1.0613 | 0.0010 | 62.0568 | 1.13e-10 | 2.6800 | 0 | 1.12 |
| 12 | 2.0000 | 0.3893 | 102.6604 | 8.34e-06 | 2.6902 | 0 | 1.10 |
| 13 | 0.5799 | 1.0000 | 60.6575 | 3.18e-19 | 2.7242 | 0 | 1.05 |
| 14 | 0.9899 | 0.0010 | 61.8311 | 2.04e-11 | 2.6800 | 0 | 1.12 |
| 15 | 1.5859 | 0.0104 | 67.6532 | 2.95e-07 | 2.6804 | 0 | 1.09 |
| 16 | 1.3293 | 0.1175 | 64.3615 | 1.37e-08 | 2.6849 | 0 | 1.07 |
| 17 | 1.6373 | 0.9787 | 128.9493 | 5.24e-07 | 2.7003 | 0 | 1.09 |
| 18 | 1.6396 | 0.2110 | 71.8825 | 5.03e-07 | 2.6879 | 0 | 1.09 |
| 19 | 1.5659 | 1.0000 | 116.1545 | 2.58e-07 | 2.7031 | 0 | 1.12 |
| 20 | 1.5992 | 0.0010 | 67.8177 | 3.37e-07 | 2.6800 | 0 | 1.05 |
| 21 | 1.7209 | 0.0010 | 70.6279 | 1.03e-06 | 2.6800 | 0 | 1.09 |
| 22 | 1.4825 | 0.0010 | 65.7644 | 9.70e-08 | 2.6800 | 0 | 1.05 |
| 23 | 0.9516 | 0.7338 | 62.7530 | 7.45e-12 | 2.7113 | 0 | 1.06 |
| 24 | 2.0000 | 0.4382 | 107.7652 | 8.38e-06 | 2.6909 | 0 | 1.09 |
| 25 | 1.8135 | 0.4195 | 87.5358 | 2.25e-06 | 2.6928 | 0 | 1.08 |
| 26 | 1.9840 | 0.5166 | 115.4251 | 7.62e-06 | 2.6920 | 0 | 1.08 |
| 27 | 0.5000 | 0.0010 | 61.4825 | 3.03e-22 | 2.6800 | 0 | 1.06 |
| 28 | 1.5456 | 0.9301 | 101.8398 | 2.07e-07 | 2.7045 | 0 | 1.07 |
| 29 | 0.6483 | 0.7074 | 60.9014 | 3.10e-17 | 2.7111 | 0 | 1.10 |
| 30 | 1.7436 | 0.0905 | 72.8448 | 1.26e-06 | 2.6833 | 0 | 1.10 |

B.1.2. KC200GT (Polycrystalline)

Table B.14: Optimal parameters for single-diode model of KC200GT using BMR.

| Run | a | R_s (Ω) | R_p (Ω) | I_0 (A) | I_{pv} (A) | ERR | Time(s) |
|-----|--------|--------------------|--------------------|-----------|--------------|-----|---------|
| 1 | 1.2335 | 0.2097 | 154.1243 | 3.59e-08 | 8.2212 | 0 | 2.10 |
| 2 | 0.5000 | 0.4512 | 50.0000 | 1.93e-20 | 8.2841 | 0 | 2.18 |
| 3 | 0.8299 | 0.1710 | 50.0000 | 2.96e-12 | 8.2381 | 0 | 2.12 |
| 4 | 1.3286 | 0.0308 | 74.2163 | 1.38e-07 | 8.2134 | 0 | 2.15 |
| 5 | 0.5899 | 0.3753 | 50.0000 | 2.65e-17 | 8.2716 | 0 | 2.09 |
| 6 | 1.0272 | 0.0010 | 50.0000 | 7.12e-10 | 8.2102 | 0 | 2.30 |
| 7 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.13 |
| 8 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.19 |
| 9 | 0.8156 | 0.1833 | 50.0000 | 1.79e-12 | 8.2401 | 0 | 2.11 |
| 10 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.11 |
| 11 | 1.2140 | 0.1087 | 75.5858 | 2.56e-08 | 8.2218 | 0 | 2.22 |
| 12 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.10 |
| 13 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.12 |
| 14 | 1.4639 | 0.0324 | 103.3724 | 7.29e-07 | 8.2126 | 0 | 2.14 |
| 15 | 1.5080 | 0.0141 | 107.2939 | 1.17e-06 | 8.2111 | 0 | 2.20 |
| 16 | 0.8131 | 0.1854 | 50.0000 | 1.64e-12 | 8.2404 | 0 | 2.17 |
| 17 | 1.1749 | 0.0947 | 67.2581 | 1.33e-08 | 8.2216 | 0 | 0.25 |
| 18 | 1.0273 | 0.0010 | 50.0000 | 7.14e-10 | 8.2102 | 0 | 2.14 |
| 19 | 1.5781 | 0.0303 | 160.7382 | 2.38e-06 | 8.2115 | 0 | 2.21 |
| 20 | 1.3139 | 0.0010 | 67.0030 | 1.12e-07 | 8.2101 | 0 | 2.09 |
| 21 | 0.8202 | 0.1793 | 50.0000 | 2.11e-12 | 8.2394 | 0 | 2.19 |
| 22 | 0.5000 | 0.4512 | 50.0000 | 1.93e-20 | 8.2841 | 0 | 2.17 |
| 23 | 1.6711 | 0.0010 | 200.0000 | 5.53e-06 | 8.2100 | 0 | 2.16 |
| 24 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.21 |
| 25 | 0.5000 | 0.4512 | 50.0000 | 1.93e-20 | 8.2841 | 0 | 2.11 |
| 26 | 0.6895 | 0.4978 | 147.6295 | 9.29e-15 | 8.2377 | 0 | 2.18 |
| 27 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.15 |
| 28 | 0.6294 | 0.4180 | 58.3483 | 3.35e-16 | 8.2688 | 0 | 2.20 |
| 29 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 2.16 |
| 30 | 0.5000 | 0.4512 | 50.0000 | 1.93e-20 | 8.2841 | 0 | 2.09 |

B.1.3. Shell SQ85 (Monocrystalline)

Table B.15: Optimal parameters for single-diode model of *Shell SQ85* using BMR.

| Run | a | R_s (Ω) | R_p (Ω) | I_0 (A) | I_{pv} (A) | ERR | Time(s) |
|-----|--------|--------------------|--------------------|-----------|--------------|-----|---------|
| 1 | 1.4689 | 0.0588 | 50.0000 | 4.01e-07 | 5.4564 | 0 | 2.21 |
| 2 | 1.1542 | 0.4138 | 100.3448 | 4.89e-09 | 5.4725 | 0 | 2.35 |
| 3 | 0.5935 | 0.6425 | 53.6518 | 1.39e-17 | 5.5153 | 0 | 2.14 |
| 4 | 1.5322 | 0.2053 | 91.9249 | 8.22e-07 | 5.4622 | 0 | 2.17 |
| 5 | 2.0000 | 0.0010 | 117.3588 | 3.23e-05 | 5.4500 | 0 | 2.27 |
| 6 | 0.8211 | 0.5962 | 117.5789 | 1.07e-12 | 5.4776 | 0 | 2.20 |
| 7 | 1.0590 | 0.4835 | 130.8259 | 7.61e-10 | 5.4701 | 0 | 2.18 |
| 8 | 1.1356 | 0.3938 | 78.9634 | 3.44e-09 | 5.4772 | 0 | 2.14 |
| 9 | 1.0203 | 0.3601 | 51.1177 | 3.07e-10 | 5.4884 | 0 | 2.30 |
| 10 | 1.6575 | 0.0010 | 56.2860 | 2.60e-06 | 5.4501 | 0 | 2.21 |
| 11 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 2.16 |
| 12 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 2.17 |
| 13 | 2.0000 | 0.0010 | 117.3608 | 3.23e-05 | 5.4500 | 0 | 2.15 |
| 14 | 1.9249 | 0.0010 | 93.0542 | 2.00e-05 | 5.4501 | 0 | 2.21 |
| 15 | 1.3866 | 0.1126 | 50.0000 | 1.52e-07 | 5.4623 | 0 | 2.16 |
| 16 | 1.6135 | 0.2250 | 160.5309 | 1.84e-06 | 5.4576 | 0 | 2.17 |
| 17 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 2.15 |
| 18 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 2.16 |
| 19 | 1.1650 | 0.3838 | 82.1909 | 5.88e-09 | 5.4754 | 0 | 2.21 |
| 20 | 1.0862 | 0.4837 | 167.5087 | 1.35e-09 | 5.4657 | 0 | 2.19 |
| 21 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 2.32 |
| 22 | 1.6318 | 0.0010 | 54.4721 | 2.06e-06 | 5.4501 | 0 | 2.24 |
| 23 | 1.6357 | 0.0847 | 68.1981 | 2.17e-06 | 5.4568 | 0 | 2.19 |
| 24 | 1.9857 | 0.0010 | 111.6965 | 2.96e-05 | 5.4500 | 0 | 2.16 |
| 25 | 1.7333 | 0.1131 | 99.6851 | 5.07e-06 | 5.4562 | 0 | 2.19 |
| 26 | 2.0000 | 0.0010 | 117.3644 | 3.23e-05 | 5.4500 | 0 | 2.13 |
| 27 | 1.5085 | 0.2817 | 174.6899 | 6.56e-07 | 5.4588 | 0 | 2.19 |
| 28 | 1.8213 | 0.1081 | 135.7114 | 1.00e-05 | 5.4543 | 0 | 2.16 |
| 29 | 2.0000 | 0.0010 | 117.3648 | 3.23e-05 | 5.4500 | 0 | 2.16 |
| 30 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 2.16 |

B.2. Double-Diode Model

B.2.1. Shell ST40

Table B.16: Optimal parameters for double-diode model of *Shell ST40* using BMR.

| Run | a_1 | a_2 | R_s (Ω) | R_p (Ω) | I_{o1} (A) | I_{o2} (A) | I_{pv} (A) | ERR | Time (s) |
|-----|--------|--------|--------------------|--------------------|--------------|--------------|--------------|-----|----------|
| 1 | 1.8058 | 0.5400 | 0.0853 | 61.5221 | 2.33e-08 | 2.33e-07 | 2.7336 | 0 | 3.42 |
| 2 | 1.3373 | 0.5131 | 0.6560 | 61.1905 | 6.43e-10 | 6.43e-09 | 2.7336 | 0 | 3.41 |
| 3 | 1.5001 | 0.5690 | 0.7703 | 60.8911 | 9.28e-10 | 9.28e-09 | 2.7336 | 0 | 3.62 |
| 4 | 1.9850 | 1.2160 | 0.1123 | 64.9245 | 8.19e-07 | 8.19e-06 | 2.7336 | 0 | 3.41 |
| 5 | 1.9686 | 1.9527 | 0.0147 | 78.8740 | 1.29e-07 | 1.29e-06 | 2.7336 | 0 | 3.55 |
| 6 | 2.0000 | 1.1818 | 0.0011 | 63.2981 | 3.73e-07 | 3.73e-06 | 2.7336 | 0 | 3.56 |
| 7 | 1.9009 | 0.6732 | 0.0043 | 62.3127 | 2.82e-07 | 2.82e-06 | 2.7336 | 0 | 3.41 |
| 8 | 1.8046 | 0.6559 | 0.0012 | 61.5503 | 1.27e-08 | 1.27e-07 | 2.7336 | 0 | 3.39 |
| 9 | 1.7336 | 0.7306 | 0.2492 | 61.2966 | 1.10e-10 | 1.10e-09 | 2.7336 | 0 | 3.43 |
| 10 | 1.8438 | 1.2757 | 0.4013 | 69.5939 | 6.37e-07 | 6.37e-06 | 2.7336 | 0 | 3.38 |
| 11 | 1.8817 | 0.7195 | 0.8286 | 68.4645 | 6.67e-07 | 6.67e-06 | 2.7336 | 0 | 3.43 |
| 12 | 1.6417 | 0.9601 | 0.0464 | 62.7288 | 7.28e-08 | 7.28e-07 | 2.7336 | 0 | 3.47 |
| 13 | 1.9109 | 0.6367 | 0.5365 | 61.0902 | 1.62e-08 | 1.62e-07 | 2.7336 | 0 | 3.52 |
| 14 | 1.9979 | 1.8750 | 0.3619 | 89.8570 | 8.07e-07 | 8.07e-06 | 2.7336 | 0 | 3.49 |
| 15 | 1.9451 | 1.0114 | 0.2289 | 62.9991 | 3.21e-07 | 3.21e-06 | 2.7336 | 0 | 3.46 |
| 16 | 1.8983 | 0.5168 | 0.9749 | 65.1987 | 3.94e-07 | 3.94e-06 | 2.7336 | 0 | 3.35 |
| 17 | 1.8494 | 0.8759 | 0.4822 | 68.3785 | 8.46e-07 | 8.46e-06 | 2.7336 | 0 | 3.38 |
| 18 | 1.9990 | 0.5004 | 0.1796 | 62.0005 | 3.03e-07 | 3.03e-06 | 2.7336 | 0 | 3.43 |
| 19 | 1.0596 | 0.5743 | 0.6046 | 61.0786 | 7.86e-12 | 7.86e-11 | 2.7336 | 0 | 3.44 |
| 20 | 1.9981 | 0.7187 | 0.2286 | 63.5699 | 8.99e-07 | 8.99e-06 | 2.7336 | 0 | 3.40 |
| 21 | 1.9104 | 0.9900 | 0.2515 | 62.4151 | 1.32e-07 | 1.32e-06 | 2.7336 | 0 | 3.43 |
| 22 | 1.9982 | 0.5806 | 0.5260 | 61.7996 | 2.28e-07 | 2.28e-06 | 2.7336 | 0 | 3.46 |
| 23 | 1.8468 | 1.1143 | 0.0249 | 62.6831 | 1.01e-07 | 1.01e-06 | 2.7336 | 0 | 3.39 |
| 24 | 1.8770 | 0.6487 | 0.0039 | 61.9505 | 1.42e-07 | 1.42e-06 | 2.7336 | 0 | 3.53 |
| 25 | 1.8873 | 1.7321 | 0.9991 | 197.3223 | 9.92e-07 | 9.92e-06 | 2.7336 | 0 | 3.31 |
| 26 | 1.7121 | 0.8316 | 0.0300 | 61.5462 | 1.90e-10 | 1.90e-09 | 2.7336 | 0 | 3.40 |
| 27 | 1.9898 | 0.5160 | 0.3087 | 61.2051 | 1.05e-08 | 1.05e-07 | 2.7336 | 0 | 3.40 |
| 28 | 1.9476 | 1.8044 | 0.0016 | 73.0430 | 4.23e-09 | 4.23e-08 | 2.7336 | 0 | 3.46 |
| 29 | 1.9144 | 0.5180 | 0.1926 | 63.6196 | 6.45e-07 | 6.45e-06 | 2.7336 | 0 | 3.41 |
| 30 | 1.9057 | 1.4162 | 0.9028 | 86.6527 | 1.66e-07 | 1.66e-06 | 2.7336 | 0 | 3.38 |

B.2.2. KC200GT (Polycrystalline)

Table B.17: Optimal parameters for double-diode model of KC200GT using BMR.

| Run | a_1 | a_2 | R_s (Ω) | R_p (Ω) | I_{o1} (A) | I_{o2} (A) | I_{pv} (A) | ERR | Time (s) |
|-----|--------|--------|--------------------|--------------------|--------------|--------------|--------------|-----|----------|
| 1 | 1.0442 | 0.7540 | 0.0024 | 50.0166 | 9.41e-10 | 9.41e-09 | 8.3742 | 0 | 3.58 |
| 2 | 1.5324 | 0.5411 | 0.0022 | 50.1624 | 3.15e-07 | 3.15e-06 | 8.3742 | 0 | 3.56 |
| 3 | 1.2637 | 0.7330 | 0.3648 | 64.4453 | 1.18e-09 | 1.18e-08 | 8.3742 | 0 | 3.56 |
| 4 | 1.3547 | 0.5653 | 0.3753 | 50.8742 | 4.51e-09 | 4.51e-08 | 8.3742 | 0 | 3.78 |
| 5 | 1.6971 | 0.7447 | 0.0865 | 50.2869 | 5.99e-07 | 5.99e-06 | 8.3742 | 0 | 3.63 |
| 6 | 1.4099 | 0.8363 | 0.0015 | 53.9622 | 1.39e-07 | 1.39e-06 | 8.3742 | 0 | 3.70 |
| 7 | 1.6879 | 0.7222 | 0.0089 | 50.8575 | 9.48e-07 | 9.48e-06 | 8.3742 | 0 | 3.61 |
| 8 | 1.6767 | 0.5001 | 0.0212 | 50.0274 | 8.49e-07 | 8.49e-06 | 8.3742 | 0 | 3.68 |
| 9 | 1.1478 | 1.2168 | 0.1624 | 95.2183 | 5.38e-10 | 5.38e-09 | 8.3742 | 0 | 3.59 |
| 10 | 1.5935 | 0.8158 | 0.0013 | 52.7692 | 5.71e-07 | 5.71e-06 | 8.3742 | 0 | 3.55 |
| 11 | 1.5624 | 0.5202 | 0.0020 | 50.0099 | 3.93e-07 | 3.93e-06 | 8.3742 | 0 | 3.69 |
| 12 | 1.4106 | 1.0002 | 0.1350 | 189.8023 | 3.97e-07 | 3.97e-06 | 8.3742 | 0 | 3.66 |
| 13 | 1.9617 | 0.9775 | 0.0565 | 50.9805 | 2.86e-07 | 2.86e-06 | 8.3742 | 0 | 3.72 |
| 14 | 1.6817 | 1.1436 | 0.2558 | 192.5735 | 3.24e-07 | 3.24e-06 | 8.3742 | 0 | 3.58 |
| 15 | 1.7331 | 1.0090 | 0.2869 | 112.0015 | 2.77e-07 | 2.77e-06 | 8.3742 | 0 | 3.58 |
| 16 | 1.8675 | 1.0924 | 0.1423 | 71.0451 | 8.98e-07 | 8.98e-06 | 8.3742 | 0 | 3.57 |
| 17 | 1.3034 | 0.7743 | 0.0213 | 55.3038 | 5.11e-08 | 5.11e-07 | 8.3742 | 0 | 3.66 |
| 18 | 1.8175 | 0.9292 | 0.0417 | 50.2220 | 5.46e-07 | 5.46e-06 | 8.3742 | 0 | 3.69 |
| 19 | 1.8239 | 0.8099 | 0.0858 | 50.0437 | 9.36e-07 | 9.36e-06 | 8.3742 | 0 | 3.63 |
| 20 | 1.8817 | 1.0208 | 0.0013 | 50.3330 | 2.60e-07 | 2.60e-06 | 8.3742 | 0 | 3.68 |
| 21 | 1.5080 | 1.3947 | 0.0058 | 96.3903 | 9.30e-07 | 9.30e-06 | 8.3742 | 0 | 3.61 |
| 22 | 1.3791 | 1.5716 | 0.0232 | 115.2074 | 8.60e-08 | 8.60e-07 | 8.3742 | 0 | 3.70 |
| 23 | 1.6937 | 0.5334 | 0.0347 | 50.2006 | 9.27e-07 | 9.27e-06 | 8.3742 | 0 | 3.72 |
| 24 | 1.8250 | 1.0250 | 0.0014 | 50.0239 | 2.96e-08 | 2.96e-07 | 8.3742 | 0 | 3.62 |
| 25 | 1.6332 | 1.1632 | 0.0766 | 72.8047 | 5.65e-07 | 5.65e-06 | 8.3742 | 0 | 3.62 |
| 26 | 1.5927 | 1.4287 | 0.0388 | 105.7836 | 4.94e-07 | 4.94e-06 | 8.3742 | 0 | 3.60 |
| 27 | 1.3895 | 1.7823 | 0.0140 | 80.8836 | 2.96e-07 | 2.96e-06 | 8.3742 | 0 | 3.66 |
| 28 | 1.6611 | 1.0456 | 0.0071 | 59.3309 | 9.69e-07 | 9.69e-06 | 8.3742 | 0 | 3.70 |
| 29 | 1.8807 | 0.5413 | 0.5266 | 87.4063 | 5.25e-07 | 5.25e-06 | 8.3742 | 0 | 3.72 |
| 30 | 1.4941 | 0.7963 | 0.0036 | 50.2907 | 1.87e-07 | 1.87e-06 | 8.3742 | 0 | 3.55 |

B.2.3. Shell SQ85

Table B.18: Optimal parameters for double-diode model of *Shell SQ85* using BMR.

| Run | a_1 | a_2 | R_s (Ω) | R_p (Ω) | I_{o1} (A) | I_{o2} (A) | I_{pv} (A) | ERR | Time (s) |
|-----|--------|--------|--------------------|--------------------|--------------|--------------|--------------|-----|----------|
| 1 | 1.9814 | 1.9727 | 0.0105 | 113.9955 | 3.70e-07 | 3.70e-06 | 5.5590 | 0 | 3.50 |
| 2 | 1.9408 | 1.9999 | 0.0019 | 116.9629 | 9.81e-07 | 9.81e-06 | 5.5590 | 0 | 3.46 |
| 3 | 1.2354 | 0.7562 | 0.5196 | 50.1373 | 1.95e-10 | 1.95e-09 | 5.5590 | 0 | 3.49 |
| 4 | 1.5205 | 0.5061 | 0.1951 | 63.4326 | 5.65e-07 | 5.65e-06 | 5.5590 | 0 | 3.53 |
| 5 | 1.7931 | 1.8558 | 0.0153 | 82.7090 | 5.89e-07 | 5.89e-06 | 5.5590 | 0 | 3.41 |
| 6 | 1.5208 | 1.7861 | 0.0033 | 50.2814 | 6.10e-07 | 6.10e-06 | 5.5590 | 0 | 3.42 |
| 7 | 1.4919 | 1.9592 | 0.0642 | 66.1392 | 3.59e-07 | 3.59e-06 | 5.5590 | 0 | 3.40 |
| 8 | 1.6568 | 1.4611 | 0.1615 | 64.0911 | 1.09e-07 | 1.09e-06 | 5.5590 | 0 | 3.40 |
| 9 | 1.6396 | 1.3746 | 0.2843 | 94.0951 | 1.11e-07 | 1.11e-06 | 5.5590 | 0 | 3.43 |
| 10 | 1.8194 | 0.8179 | 0.4848 | 50.4412 | 1.05e-08 | 1.05e-07 | 5.5590 | 0 | 3.37 |
| 11 | 1.6070 | 1.7884 | 0.0023 | 61.0064 | 7.19e-07 | 7.19e-06 | 5.5590 | 0 | 3.41 |
| 12 | 1.3648 | 1.6856 | 0.0134 | 59.4834 | 3.63e-09 | 3.63e-08 | 5.5590 | 0 | 3.44 |
| 13 | 1.7450 | 1.4752 | 0.0555 | 50.1234 | 1.59e-08 | 1.59e-07 | 5.5590 | 0 | 3.61 |
| 14 | 1.5515 | 0.5551 | 0.6996 | 128.4673 | 6.71e-08 | 6.71e-07 | 5.5590 | 0 | 3.37 |
| 15 | 1.9181 | 1.5487 | 0.0082 | 50.1358 | 1.30e-09 | 1.30e-08 | 5.5590 | 0 | 3.36 |
| 16 | 1.5561 | 0.5003 | 0.0216 | 50.8919 | 9.72e-07 | 9.72e-06 | 5.5590 | 0 | 3.42 |
| 17 | 1.6984 | 1.9879 | 0.0011 | 93.3368 | 8.57e-07 | 8.57e-06 | 5.5590 | 0 | 3.45 |
| 18 | 1.6286 | 0.5351 | 0.7525 | 199.0567 | 8.69e-09 | 8.69e-08 | 5.5590 | 0 | 3.48 |
| 19 | 1.7609 | 1.5185 | 0.0301 | 51.0622 | 2.95e-07 | 2.95e-06 | 5.5590 | 0 | 3.39 |
| 20 | 1.8198 | 1.5543 | 0.0091 | 50.9701 | 2.59e-07 | 2.59e-06 | 5.5590 | 0 | 3.52 |
| 21 | 1.7426 | 0.5787 | 0.5143 | 64.9985 | 9.37e-07 | 9.37e-06 | 5.5590 | 0 | 3.44 |
| 22 | 1.6035 | 1.7609 | 0.0552 | 65.6268 | 9.88e-07 | 9.88e-06 | 5.5590 | 0 | 3.38 |
| 23 | 1.6979 | 0.5577 | 0.6590 | 199.7395 | 5.66e-07 | 5.66e-06 | 5.5590 | 0 | 3.45 |
| 24 | 1.7630 | 1.8605 | 0.0011 | 78.3176 | 4.79e-07 | 4.79e-06 | 5.5590 | 0 | 3.52 |
| 25 | 1.6456 | 0.8651 | 0.2407 | 50.1496 | 7.34e-07 | 7.34e-06 | 5.5590 | 0 | 3.36 |
| 26 | 1.7886 | 1.5626 | 0.0018 | 50.4282 | 3.34e-08 | 3.34e-07 | 5.5590 | 0 | 3.44 |
| 27 | 1.6893 | 1.4621 | 0.0619 | 51.6681 | 4.15e-07 | 4.15e-06 | 5.5590 | 0 | 3.42 |
| 28 | 1.6585 | 0.8123 | 0.4781 | 53.5873 | 1.07e-07 | 1.07e-06 | 5.5590 | 0 | 3.37 |
| 29 | 1.3981 | 1.9936 | 0.0219 | 90.7298 | 4.13e-08 | 4.13e-07 | 5.5590 | 0 | 3.43 |
| 30 | 1.9967 | 1.9727 | 0.0184 | 120.5958 | 3.15e-07 | 3.15e-06 | 5.5590 | 0 | 3.48 |

C. JAYA Algorithm

C.1. Single-Diode Model

C.1.1. Shell ST40 (Thin-Film)

Table C.19: Optimal parameters for single-diode model of *Shell ST40* using JAYA.

| Run | a | R_s (Ω) | R_p (Ω) | I_0 (A) | I_{pv} (A) | ERR | Time(s) |
|-----|--------|--------------------|--------------------|-----------|--------------|-----|---------|
| 1 | 2.0000 | 0.3740 | 101.2313 | 8.33e-06 | 2.6899 | 0 | 1.46 |
| 2 | 1.0825 | 0.0010 | 62.1405 | 1.80e-10 | 2.6800 | 0 | 0.14 |
| 3 | 0.6895 | 0.7133 | 60.9815 | 3.16e-16 | 2.7113 | 0 | 1.53 |
| 4 | 1.0259 | 0.9791 | 66.5231 | 5.13e-11 | 2.7194 | 0 | 0.79 |
| 5 | 0.5187 | 0.2947 | 61.1888 | 1.86e-21 | 2.6929 | 0 | 0.38 |
| 6 | 1.3434 | 0.0010 | 63.9836 | 1.66e-08 | 2.6800 | 0 | 3.14 |
| 7 | 2.0000 | 0.7718 | 200.0000 | 8.72e-06 | 2.6904 | 0 | 0.47 |
| 8 | 0.5000 | 0.1188 | 61.3632 | 3.03e-22 | 2.6852 | 0 | 1.87 |
| 9 | 2.0000 | 0.0010 | 80.5768 | 8.10e-06 | 2.6800 | 0 | 0.35 |
| 10 | 2.0000 | 0.0010 | 80.5767 | 8.10e-06 | 2.6800 | 0 | 0.48 |
| 11 | 2.0000 | 0.5319 | 120.6052 | 8.46e-06 | 2.6918 | 0 | 3.91 |
| 12 | 1.8328 | 0.4822 | 93.1398 | 2.62e-06 | 2.6939 | 0 | 3.84 |
| 13 | 0.5630 | 0.3900 | 61.0997 | 8.56e-20 | 2.6971 | 0 | 0.15 |
| 14 | 0.7340 | 0.4268 | 61.1783 | 2.88e-15 | 2.6987 | 0 | 0.32 |
| 15 | 1.4660 | 0.0010 | 65.5177 | 8.01e-08 | 2.6800 | 0 | 0.58 |
| 16 | 0.5000 | 1.0000 | 60.5306 | 3.08e-22 | 2.7243 | 0 | 0.14 |
| 17 | 0.7306 | 0.0010 | 61.5065 | 2.44e-15 | 2.6800 | 0 | 0.51 |
| 18 | 1.9670 | 0.7209 | 158.2633 | 6.98e-06 | 2.6922 | 0 | 1.57 |
| 19 | 1.8610 | 0.0010 | 74.9031 | 3.13e-06 | 2.6800 | 0 | 2.42 |
| 20 | 1.7730 | 1.0000 | 200.0000 | 1.74e-06 | 2.6934 | 0 | 1.36 |
| 21 | 0.5959 | 0.0010 | 61.4833 | 1.00e-18 | 2.6800 | 0 | 0.23 |
| 22 | 0.5000 | 0.3838 | 61.0997 | 3.05e-22 | 2.6968 | 0 | 1.65 |
| 23 | 1.6184 | 1.0000 | 129.0635 | 4.38e-07 | 2.7008 | 0 | 1.48 |
| 24 | 1.7677 | 1.0000 | 196.1318 | 1.67e-06 | 2.6937 | 0 | 0.45 |
| 25 | 0.6312 | 0.7999 | 60.8296 | 1.08e-17 | 2.7152 | 0 | 0.10 |
| 26 | 1.6288 | 0.9391 | 118.2015 | 4.81e-07 | 2.7013 | 0 | 3.98 |
| 27 | 0.5000 | 0.9505 | 60.5689 | 3.08e-22 | 2.7221 | 0 | 0.08 |
| 28 | 1.5517 | 0.7643 | 87.4583 | 2.17e-07 | 2.7034 | 0 | 2.71 |
| 29 | 1.4889 | 0.6435 | 77.1432 | 1.08e-07 | 2.7024 | 0 | 2.52 |
| 30 | 2.0000 | 0.5645 | 126.3554 | 8.49e-06 | 2.6920 | 0 | 3.93 |

C.1.2. KC200GT (Polycrystalline)

Table C.20: Optimal parameters for single-diode model of KC200GT using JAYA.

| Run | a | R_s (Ω) | R_p (Ω) | I_0 (A) | I_{pv} (A) | ERR | Time(s) |
|-----|--------|--------------------|--------------------|-----------|--------------|-----|---------|
| 1 | 1.4382 | 0.0010 | 84.1046 | 5.40e-07 | 8.2101 | 0 | 0.79 |
| 2 | 1.5794 | 0.0010 | 126.7525 | 2.40e-06 | 8.2101 | 0 | 0.77 |
| 3 | 1.2164 | 0.1346 | 83.9885 | 2.68e-08 | 8.2232 | 0 | 0.76 |
| 4 | 0.5000 | 0.5392 | 67.0968 | 1.97e-20 | 8.2760 | 0 | 0.77 |
| 5 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 0.80 |
| 6 | 1.6337 | 0.0010 | 161.0948 | 3.98e-06 | 8.2101 | 0 | 0.81 |
| 7 | 1.6589 | 0.0073 | 200.0000 | 4.98e-06 | 8.2103 | 0 | 0.87 |
| 8 | 1.5897 | 0.0010 | 131.9580 | 2.65e-06 | 8.2101 | 0 | 0.73 |
| 9 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 0.79 |
| 10 | 1.6614 | 0.0020 | 190.3854 | 5.09e-06 | 8.2101 | 0 | 0.79 |
| 11 | 1.6711 | 0.0010 | 200.0000 | 5.53e-06 | 8.2100 | 0 | 0.75 |
| 12 | 1.3947 | 0.0010 | 76.8853 | 3.21e-07 | 8.2101 | 0 | 0.79 |
| 13 | 1.2877 | 0.0235 | 67.8226 | 7.77e-08 | 8.2128 | 0 | 0.76 |
| 14 | 0.5000 | 0.6069 | 190.1731 | 2.04e-20 | 8.2362 | 0 | 0.75 |
| 15 | 1.3580 | 0.0010 | 71.9271 | 2.02e-07 | 8.2101 | 0 | 0.81 |
| 16 | 1.6712 | 0.0010 | 200.0000 | 5.53e-06 | 8.2100 | 0 | 0.87 |
| 17 | 1.6711 | 0.0010 | 200.0000 | 5.53e-06 | 8.2100 | 0 | 0.81 |
| 18 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 0.40 |
| 19 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 0.54 |
| 20 | 1.6676 | 0.0010 | 195.5287 | 5.37e-06 | 8.2100 | 0 | 0.80 |
| 21 | 1.5817 | 0.0046 | 131.2384 | 2.45e-06 | 8.2103 | 0 | 0.76 |
| 22 | 1.6381 | 0.0010 | 164.8169 | 4.14e-06 | 8.2100 | 0 | 0.81 |
| 23 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 0.70 |
| 24 | 1.6712 | 0.0010 | 200.0000 | 5.53e-06 | 8.2100 | 0 | 0.76 |
| 25 | 1.6443 | 0.0145 | 199.0203 | 4.39e-06 | 8.2106 | 0 | 0.75 |
| 26 | 0.5792 | 0.3844 | 50.0000 | 1.26e-17 | 8.2731 | 0 | 0.78 |
| 27 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 0.77 |
| 28 | 1.0273 | 0.0010 | 50.0000 | 7.13e-10 | 8.2102 | 0 | 0.78 |
| 29 | 0.5000 | 0.5952 | 132.5964 | 2.02e-20 | 8.2469 | 0 | 0.76 |
| 30 | 1.6207 | 0.0019 | 152.4129 | 3.54e-06 | 8.2101 | 0 | 0.74 |

C.1.3. Shell SQ85 (Monocrystalline)

Table C.21: Optimal parameters for single-diode model of *Shell SQ85* using JAYA.

| Run | a | R_s (Ω) | R_p (Ω) | I_0 (A) | I_{pv} (A) | ERR | Time(s) |
|-----|--------|--------------------|--------------------|-----------|--------------|-----|---------|
| 1 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 0.86 |
| 2 | 2.0000 | 0.0500 | 187.6771 | 3.27e-05 | 5.4515 | 0 | 0.80 |
| 3 | 1.5570 | 0.0010 | 50.0000 | 1.01e-06 | 5.4501 | 0 | 0.77 |
| 4 | 2.0000 | 0.0010 | 117.3640 | 3.23e-05 | 5.4500 | 0 | 0.19 |
| 5 | 2.0000 | 0.0546 | 200.0000 | 3.28e-05 | 5.4515 | 0 | 0.80 |
| 6 | 2.0000 | 0.0546 | 200.0000 | 3.28e-05 | 5.4515 | 0 | 0.74 |
| 7 | 2.0000 | 0.0010 | 117.3639 | 3.23e-05 | 5.4500 | 0 | 0.74 |
| 8 | 2.0000 | 0.0402 | 166.4875 | 3.26e-05 | 5.4513 | 0 | 1.09 |
| 9 | 1.8063 | 0.1295 | 157.2574 | 9.01e-06 | 5.4545 | 0 | 0.14 |
| 10 | 2.0000 | 0.0010 | 117.3639 | 3.23e-05 | 5.4500 | 0 | 0.21 |
| 11 | 1.0856 | 0.4248 | 81.1396 | 1.30e-09 | 5.4785 | 0 | 1.03 |
| 12 | 0.7109 | 0.6633 | 155.8383 | 1.16e-14 | 5.4732 | 0 | 1.05 |
| 13 | 2.0000 | 0.0010 | 117.3634 | 3.23e-05 | 5.4500 | 0 | 1.15 |
| 14 | 1.8554 | 0.1203 | 190.0807 | 1.29e-05 | 5.4535 | 0 | 1.10 |
| 15 | 2.0000 | 0.0010 | 117.3712 | 3.23e-05 | 5.4500 | 0 | 1.18 |
| 16 | 1.7302 | 0.0010 | 62.4694 | 4.81e-06 | 5.4501 | 0 | 1.22 |
| 17 | 2.0000 | 0.0046 | 120.4674 | 3.23e-05 | 5.4502 | 0 | 1.02 |
| 18 | 1.7410 | 0.1763 | 193.3915 | 5.50e-06 | 5.4550 | 0 | 1.11 |
| 19 | 0.5000 | 0.7394 | 79.4271 | 7.42e-21 | 5.5007 | 0 | 1.05 |
| 20 | 1.0868 | 0.3585 | 57.9162 | 1.31e-09 | 5.4837 | 0 | 1.04 |
| 21 | 2.0000 | 0.0091 | 124.6253 | 3.24e-05 | 5.4504 | 0 | 1.06 |
| 22 | 2.0000 | 0.0010 | 117.3639 | 3.23e-05 | 5.4500 | 0 | 0.12 |
| 23 | 1.0795 | 0.4920 | 187.9381 | 1.18e-09 | 5.4643 | 0 | 1.02 |
| 24 | 0.5312 | 0.6724 | 51.0140 | 1.21e-19 | 5.5218 | 0 | 1.07 |
| 25 | 1.2927 | 0.1740 | 50.0000 | 4.34e-08 | 5.4690 | 0 | 1.09 |
| 26 | 2.0000 | 0.0010 | 117.3641 | 3.23e-05 | 5.4500 | 0 | 1.06 |
| 27 | 2.0000 | 0.0010 | 117.3546 | 3.23e-05 | 5.4500 | 0 | 1.11 |
| 28 | 1.5749 | 0.1055 | 65.1131 | 1.23e-06 | 5.4588 | 0 | 0.98 |
| 29 | 2.0000 | 0.0010 | 117.3643 | 3.23e-05 | 5.4500 | 0 | 1.01 |
| 30 | 1.6715 | 0.0010 | 57.3550 | 2.94e-06 | 5.4501 | 0 | 0.82 |

C.2. Double-Diode Model

C.2.1. Shell ST40

Table C.22: Optimal parameters for double-diode model of *Shell ST40* using JAYA.

| Run | a_1 | a_2 | R_s (Ω) | R_p (Ω) | I_{o1} (A) | I_{o2} (A) | I_{pv} (A) | ERR | Time (s) |
|-----|--------|--------|--------------------|--------------------|--------------|--------------|--------------|-----|----------|
| 1 | 1.7440 | 1.8783 | 0.8878 | 192.7373 | 4.67e-08 | 4.67e-07 | 2.7336 | 0 | 1.12 |
| 2 | 1.9932 | 1.9729 | 0.7742 | 185.7348 | 5.95e-07 | 5.95e-06 | 2.7336 | 0 | 0.40 |
| 3 | 1.9908 | 1.9623 | 0.7916 | 189.6419 | 4.60e-07 | 4.60e-06 | 2.7336 | 0 | 0.04 |
| 4 | 1.8832 | 0.6087 | 0.1371 | 61.4190 | 1.80e-08 | 1.80e-07 | 2.7336 | 0 | 0.17 |
| 5 | 1.8161 | 1.1433 | 0.9510 | 89.2623 | 8.14e-07 | 8.14e-06 | 2.7336 | 0 | 0.07 |
| 6 | 1.7756 | 0.8101 | 0.1824 | 65.6819 | 5.51e-07 | 5.51e-06 | 2.7336 | 0 | 0.03 |
| 7 | 1.9986 | 1.8212 | 0.9297 | 199.3614 | 9.94e-07 | 9.94e-06 | 2.7336 | 0 | 0.05 |
| 8 | 1.8902 | 1.6185 | 0.8935 | 119.1948 | 7.83e-07 | 7.83e-06 | 2.7336 | 0 | 0.12 |
| 9 | 1.8154 | 1.7569 | 0.3477 | 80.5871 | 6.15e-09 | 6.15e-08 | 2.7336 | 0 | 0.08 |
| 10 | 1.9891 | 0.7381 | 0.7366 | 63.8953 | 5.39e-07 | 5.39e-06 | 2.7336 | 0 | 0.10 |
| 11 | 1.9306 | 0.9542 | 0.5915 | 62.3667 | 2.07e-08 | 2.07e-07 | 2.7336 | 0 | 0.07 |
| 12 | 1.9835 | 1.9913 | 0.1232 | 84.7141 | 7.75e-08 | 7.75e-07 | 2.7336 | 0 | 0.03 |
| 13 | 1.9945 | 0.5298 | 0.9340 | 66.2826 | 8.44e-07 | 8.44e-06 | 2.7336 | 0 | 0.14 |
| 14 | 1.9902 | 0.9622 | 0.3596 | 63.1268 | 4.13e-07 | 4.13e-06 | 2.7336 | 0 | 0.23 |
| 15 | 1.9968 | 1.7877 | 0.9727 | 197.0536 | 3.35e-07 | 3.35e-06 | 2.7336 | 0 | 0.12 |
| 16 | 1.6823 | 1.5775 | 0.8496 | 98.2475 | 5.85e-08 | 5.85e-07 | 2.7336 | 0 | 0.05 |
| 17 | 1.9724 | 1.9896 | 0.1134 | 84.2081 | 3.80e-08 | 3.80e-07 | 2.7336 | 0 | 0.02 |
| 18 | 1.9416 | 0.6161 | 0.6517 | 63.8182 | 4.99e-07 | 4.99e-06 | 2.7336 | 0 | 0.03 |
| 19 | 1.9491 | 0.5253 | 0.1118 | 63.9703 | 9.48e-07 | 9.48e-06 | 2.7336 | 0 | 0.22 |
| 20 | 1.9987 | 0.7428 | 0.3273 | 63.9123 | 9.27e-07 | 9.27e-06 | 2.7336 | 0 | 0.06 |
| 21 | 1.9710 | 0.7699 | 0.1203 | 62.2100 | 3.23e-07 | 3.23e-06 | 2.7336 | 0 | 0.04 |
| 22 | 1.9697 | 1.4757 | 0.0676 | 66.9361 | 4.12e-07 | 4.12e-06 | 2.7336 | 0 | 0.69 |
| 23 | 1.8881 | 1.9741 | 0.5496 | 117.6460 | 2.87e-07 | 2.87e-06 | 2.7336 | 0 | 0.22 |
| 24 | 1.7908 | 1.9043 | 0.0241 | 75.9246 | 5.12e-07 | 5.12e-06 | 2.7336 | 0 | 0.04 |
| 25 | 1.9288 | 1.9906 | 0.0015 | 80.1476 | 1.10e-08 | 1.10e-07 | 2.7336 | 0 | 0.07 |
| 26 | 1.9914 | 0.5670 | 0.9990 | 60.8540 | 3.27e-08 | 3.27e-07 | 2.7336 | 0 | 0.09 |
| 27 | 1.9951 | 1.9868 | 0.7679 | 189.6890 | 6.30e-07 | 6.30e-06 | 2.7336 | 0 | 0.16 |
| 28 | 1.8174 | 1.9972 | 0.0612 | 79.0908 | 9.47e-07 | 9.47e-06 | 2.7336 | 0 | 0.22 |
| 29 | 1.9698 | 1.8235 | 0.0077 | 73.7891 | 2.49e-08 | 2.49e-07 | 2.7336 | 0 | 0.11 |
| 30 | 1.9999 | 1.4766 | 0.1494 | 66.9429 | 1.51e-08 | 1.51e-07 | 2.7336 | 0 | 0.03 |

C.2.2. KC200GT (Polycrystalline)

Table C.23: Optimal parameters for double-diode model of KC200GT using JAYA.

| Run | a_1 | a_2 | R_s (Ω) | R_p (Ω) | I_{o1} (A) | I_{o2} (A) | I_{pv} (A) | ERR | Time (s) |
|-----|--------|--------|--------------------|--------------------|--------------|--------------|--------------|-----|----------|
| 1 | 1.8418 | 0.5048 | 0.3660 | 50.0750 | 5.39e-07 | 5.39e-06 | 8.3742 | 0 | 0.42 |
| 2 | 1.8043 | 1.0700 | 0.0078 | 51.8204 | 3.12e-09 | 3.12e-08 | 8.3742 | 0 | 0.20 |
| 3 | 1.0911 | 0.5008 | 0.0510 | 50.0146 | 1.64e-09 | 1.64e-08 | 8.3742 | 0 | 1.37 |
| 4 | 1.9400 | 0.5029 | 0.3625 | 50.0478 | 9.98e-07 | 9.98e-06 | 8.3742 | 0 | 0.35 |
| 5 | 1.9760 | 1.0208 | 0.0101 | 50.7432 | 4.64e-07 | 4.64e-06 | 8.3742 | 0 | 0.08 |
| 6 | 1.7234 | 1.2739 | 0.2040 | 191.4914 | 1.05e-08 | 1.05e-07 | 8.3742 | 0 | 0.14 |
| 7 | 1.9984 | 1.6438 | 0.0085 | 190.2121 | 7.71e-07 | 7.71e-06 | 8.3742 | 0 | 0.17 |
| 8 | 1.7783 | 0.9886 | 0.0576 | 53.7316 | 5.92e-07 | 5.92e-06 | 8.3742 | 0 | 0.06 |
| 9 | 1.5559 | 1.3872 | 0.0397 | 112.9375 | 9.96e-07 | 9.96e-06 | 8.3742 | 0 | 0.34 |
| 10 | 1.9904 | 0.5543 | 0.3498 | 50.1999 | 9.94e-07 | 9.94e-06 | 8.3742 | 0 | 0.05 |
| 11 | 1.6449 | 1.4619 | 0.0644 | 147.2554 | 8.03e-07 | 8.03e-06 | 8.3742 | 0 | 1.40 |
| 12 | 1.3909 | 0.5443 | 0.0527 | 51.4128 | 8.58e-08 | 8.58e-07 | 8.3742 | 0 | 0.09 |
| 13 | 1.7225 | 1.2345 | 0.0033 | 66.6914 | 9.81e-07 | 9.81e-06 | 8.3742 | 0 | 0.32 |
| 14 | 1.7267 | 1.5955 | 0.0062 | 143.0492 | 2.32e-07 | 2.32e-06 | 8.3742 | 0 | 0.23 |
| 15 | 1.9765 | 1.0822 | 0.0111 | 52.8324 | 2.56e-07 | 2.56e-06 | 8.3742 | 0 | 0.45 |
| 16 | 1.9532 | 1.4422 | 0.0047 | 88.9666 | 9.97e-07 | 9.97e-06 | 8.3742 | 0 | 0.71 |
| 17 | 1.7814 | 0.5046 | 0.3305 | 52.8990 | 7.39e-07 | 7.39e-06 | 8.3742 | 0 | 1.06 |
| 18 | 1.9935 | 0.6489 | 0.3307 | 52.9284 | 7.82e-07 | 7.82e-06 | 8.3742 | 0 | 0.27 |
| 19 | 1.9398 | 1.6521 | 0.0016 | 179.3202 | 2.47e-08 | 2.47e-07 | 8.3742 | 0 | 0.05 |
| 20 | 1.8638 | 1.6112 | 0.0258 | 188.6960 | 2.87e-07 | 2.87e-06 | 8.3742 | 0 | 0.57 |
| 21 | 1.9792 | 0.5113 | 0.3814 | 50.3437 | 1.00e-06 | 1.00e-05 | 8.3742 | 0 | 1.06 |
| 22 | 1.9994 | 1.6047 | 0.0262 | 186.5962 | 9.57e-07 | 9.57e-06 | 8.3742 | 0 | 0.80 |
| 23 | 1.4995 | 0.9442 | 0.0444 | 50.7749 | 6.31e-08 | 6.31e-07 | 8.3742 | 0 | 0.45 |
| 24 | 1.9154 | 0.8177 | 0.4193 | 172.6346 | 9.39e-07 | 9.39e-06 | 8.3742 | 0 | 0.94 |
| 25 | 1.8270 | 0.8165 | 0.1394 | 51.4599 | 7.35e-07 | 7.35e-06 | 8.3742 | 0 | 1.01 |
| 26 | 1.5583 | 1.1831 | 0.2039 | 120.7961 | 7.91e-08 | 7.91e-07 | 8.3742 | 0 | 1.20 |
| 27 | 1.9948 | 1.0057 | 0.0019 | 50.5333 | 9.98e-07 | 9.98e-06 | 8.3742 | 0 | 0.12 |
| 28 | 1.9806 | 1.1364 | 0.0027 | 54.5812 | 8.25e-08 | 8.25e-07 | 8.3742 | 0 | 0.03 |
| 29 | 1.9329 | 1.6644 | 0.0015 | 196.9617 | 4.59e-07 | 4.59e-06 | 8.3742 | 0 | 0.61 |
| 30 | 1.9035 | 1.0206 | 0.0337 | 51.6922 | 2.81e-07 | 2.81e-06 | 8.3742 | 0 | 0.16 |

C.2.3. Shell SQ85

Table C.24: Optimal parameters for double-diode model of *Shell SQ85* using JAYA.

| Run | a_1 | a_2 | R_s (Ω) | R_p (Ω) | I_{o1} (A) | I_{o2} (A) | I_{pv} (A) | ERR | Time (s) |
|-----|--------|--------|--------------------|--------------------|--------------|--------------|--------------|-----|----------|
| 1 | 1.9946 | 1.2450 | 0.2895 | 67.8140 | 9.62e-07 | 9.62e-06 | 5.5590 | 0 | 0.25 |
| 2 | 1.9774 | 1.9837 | 0.0057 | 114.5062 | 1.19e-07 | 1.19e-06 | 5.5590 | 0 | 0.08 |
| 3 | 1.5428 | 1.6728 | 0.0062 | 52.0881 | 5.97e-07 | 5.97e-06 | 5.5590 | 0 | 0.14 |
| 4 | 1.9961 | 1.9521 | 0.0202 | 113.5314 | 4.45e-07 | 4.45e-06 | 5.5590 | 0 | 0.06 |
| 5 | 1.9356 | 0.9891 | 0.5261 | 152.4359 | 1.77e-08 | 1.77e-07 | 5.5590 | 0 | 0.04 |
| 6 | 1.9351 | 1.9967 | 0.0436 | 169.6066 | 1.58e-07 | 1.58e-06 | 5.5590 | 0 | 0.47 |
| 7 | 1.9802 | 1.9969 | 0.0083 | 122.2422 | 5.78e-07 | 5.78e-06 | 5.5590 | 0 | 0.20 |
| 8 | 1.9973 | 1.3935 | 0.0999 | 50.6567 | 9.66e-07 | 9.66e-06 | 5.5590 | 0 | 0.21 |
| 9 | 1.9901 | 1.9654 | 0.0078 | 109.2567 | 2.46e-07 | 2.46e-06 | 5.5590 | 0 | 0.13 |
| 10 | 1.9418 | 0.8608 | 0.5675 | 103.5260 | 9.48e-09 | 9.48e-08 | 5.5590 | 0 | 0.92 |
| 11 | 1.9895 | 1.3585 | 0.1649 | 55.7698 | 9.98e-07 | 9.98e-06 | 5.5590 | 0 | 0.31 |
| 12 | 1.9895 | 1.9984 | 0.0029 | 118.1495 | 9.13e-07 | 9.13e-06 | 5.5590 | 0 | 0.02 |
| 13 | 1.9860 | 1.9693 | 0.0267 | 126.9792 | 5.52e-07 | 5.52e-06 | 5.5590 | 0 | 0.11 |
| 14 | 1.8366 | 1.6321 | 0.1992 | 139.2122 | 5.42e-07 | 5.42e-06 | 5.5590 | 0 | 0.29 |
| 15 | 1.9602 | 1.4691 | 0.2251 | 84.6293 | 5.79e-09 | 5.79e-08 | 5.5590 | 0 | 0.15 |
| 16 | 1.6850 | 1.2087 | 0.3741 | 196.1184 | 8.34e-07 | 8.34e-06 | 5.5590 | 0 | 0.22 |
| 17 | 1.9143 | 1.4414 | 0.3001 | 162.2359 | 7.43e-07 | 7.43e-06 | 5.5590 | 0 | 1.66 |
| 18 | 1.9984 | 1.9807 | 0.0086 | 115.8263 | 8.41e-07 | 8.41e-06 | 5.5590 | 0 | 0.60 |
| 19 | 1.6796 | 1.6695 | 0.0111 | 58.6435 | 3.92e-07 | 3.92e-06 | 5.5590 | 0 | 0.11 |
| 20 | 1.6580 | 0.5242 | 0.6950 | 198.4982 | 3.22e-07 | 3.22e-06 | 5.5590 | 0 | 0.40 |
| 21 | 1.9625 | 1.9985 | 0.0013 | 116.9369 | 4.60e-08 | 4.60e-07 | 5.5590 | 0 | 0.35 |
| 22 | 1.9964 | 1.6937 | 0.0791 | 76.1287 | 4.24e-07 | 4.24e-06 | 5.5590 | 0 | 0.06 |
| 23 | 1.9998 | 1.9425 | 0.0809 | 199.0605 | 9.95e-07 | 9.95e-06 | 5.5590 | 0 | 0.22 |
| 24 | 1.8956 | 1.8775 | 0.1095 | 190.4242 | 5.61e-07 | 5.61e-06 | 5.5590 | 0 | 0.34 |
| 25 | 1.8919 | 1.7791 | 0.0313 | 75.9220 | 6.23e-07 | 6.23e-06 | 5.5590 | 0 | 0.15 |
| 26 | 1.9529 | 1.4395 | 0.0657 | 50.3393 | 9.34e-07 | 9.34e-06 | 5.5590 | 0 | 0.16 |
| 27 | 1.9888 | 0.5009 | 0.6644 | 51.0699 | 6.70e-07 | 6.70e-06 | 5.5590 | 0 | 0.07 |
| 28 | 1.5650 | 1.4428 | 0.0035 | 50.0968 | 9.99e-07 | 9.99e-06 | 5.5590 | 0 | 0.52 |
| 29 | 1.9515 | 1.9982 | 0.0225 | 137.8560 | 2.62e-07 | 2.62e-06 | 5.5590 | 0 | 0.39 |
| 30 | 1.6469 | 1.8516 | 0.0738 | 99.2042 | 5.47e-07 | 5.47e-06 | 5.5590 | 0 | 0.14 |